

ITTC Symbols and Terminology List

Version 2021

June 2021

Supersedes all previous versions

Updated by the 29th ITTC Quality Systems Group

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NOTE: bold letters are used to denote vectors Red colour identifies the additions/modifications of this ver4sion of the List

1.1.1 Uncertainty

ITTC	Computer	Nama	Definition or	SI-
Symbol	Symbol	Name	Explanation	Unit

1. **GENERAL**

Fundamental Concepts 1.1

1.1.1 Uncertainty (The following table follows ISO/IEC Guide 98-3:2008 – Annex J)

(The following table fo	ollows ISO/IEC Guide 98-3:2008 – Annex J)		
а	Half-width of a rectangular distribution	Half-width of a rectangular distribution of possible values of input quantity X_i : $a = (a_+ - a) / 2$	
<i>a</i> +	Upper bound	Upper bound, or upper limit, of input quantity X_i :	
a_	Lower bound	Lower bound, or lower limit, of input quantity X_i :	
b_{+}	Upper bound of the deviation	Upper bound, or upper limit, of the deviation of input quantity X_i from its estimate x_i : $b_+ = a_+ - x_i$	
b_	Lower bound of the deviation	Lower bound, or lower limit, of the deviation of input quantity X_i from its estimate x_i : $b = x_i - a$	
c_i	Sensitivity coefficient	$c_i = \partial f/\partial x_i$.	1
f	Function	Functional relationship between measurand Y and input quantities X_i on which Y depends, and between output estimate y and input estimates x_i on which y depends.	1
$\partial f/\partial x_i$	Partial derivative	Partial derivative of f with respect to input quantity x_i	1
k	Coverage factor	For calculation of expanded uncertainty $U = ku_c(y)$	1
k_p	Coverage factor for probability p	For calculation of expanded uncertainty $U_p = k_p u_c(y)$	1
n	Number of repeated observations	• • • • • • • • • • • • • • • • • • • •	1
N	Number of input quantities	Number of input quantities X_i on which the measurand Y depends	1
p	Probability	Level of confidence: $0 \le p \le 1.0$	1
\overline{q}	Random quantity		1
\overline{q}	Arithmetic mean or average		1
q_k	kth observation of q	k th independent repeated observation of randomly varying quantity q	1
$r(x_i,x_j)$	Estimated correlation coefficient	$r(x_i, x_j) = u(x_i, x_j)/(u(x_i) u(x_j))$	1
$S_{\rm p}^2$	Pooled estimate of variance		1
Sp	Pooled experimental standard deviation	Positive square root of S_p^2	1
$s^2(\overline{q})$	Experimental variance of the mean	$s^2(\overline{q}) = s^2(q_k)/n$; estimated variance obtained from a Type A evaluation	1
$s(\overline{q})$	Experimental standard deviation of the mean	Positive square root of $s^2(\overline{q})$	1
$s^2(q_k)$	Experimental variance from repeated observations		1

1.1.1 Uncertainty

ITTC	Computer	Name	Definition or	SI-
Symbol	Symbol	- Traine	Explanation	Unit
$s(q_k)$		Experimental standard deviation of repeated observations	Positive square root of $s^2(q_k)$	1
$s^2(\overline{X}_i)$		Experimental variance of input mean	From mean \overline{X}_i , determined from n independent repeated observations $X_{i,k}$, estimated variance obtained from a Type A evaluation.	1
$s(\overline{X}_i)$		Standard deviation of input mean	Positive square root of $s^2(\overline{X}_1)$	1
$s(\overline{q},\overline{r})$		Estimate of covariance of means		1
$s(\overline{X}_i, \overline{X}_j)$		Estimate of covariance of input means		1
$t_p(v)$		Inverse Student t	Student <i>t</i> -distribution for <i>v</i> degrees of freedom corresponding to a given probability <i>p</i>	1
$t_p(v_{ m eff})$		Inverse Student <i>t</i> for effective degrees of freedom	Student <i>t</i> -distribution for v_{eff} degrees of freedom corresponding to a given probability p in calculation of expanded uncertainty U_p	1
$u^2(x_i)$		Estimated variance	Associated with input estimate x_i that estimates input quantity X_i	1
$u(x_i)$		Standard deviation	Positive square root of $u^2(x_i)$	1
$u(x_i,x_j)$		Estimated covariance		1
$u_{\rm c}^2(y)$		Combined variance	Combined variance associated with output estimate <i>y</i>	1
$u_{c}(y)$		Combined standard uncertainty	Positive square root of $u_c^2(y)$	1
$u_{cA}(y)$		Combined standard uncertainty from Type A	From Type A evaluations alone	1
$u_{cB}(y)$		Combined standard uncertainty from Type B	From Type B evaluations alone	1
$u_c(y_i)$		Combined standard uncertainty	Combined standard uncertainty of output estimate y_i when two or more measurands or output quantities are determined in the same measurement	1
$u_i^2(y)$		Component of combined variance	$u_i^2(y) \equiv [c_i u(x_i)]^2$	1
$_{I}u_{i}(y)$		Component of combined standard uncertainty	$u_i(y) \equiv c_i u(x_i)$	1
$u(x_i)/ x_i $		Relative standard uncertainty of output estimate <i>x</i>		1
$u_c(y)/ y $		Relative combined standard uncertainty of output estimate <i>y</i>		
$[u(x_i)/ x_i]^2$		Estimated relative variance	Estimated relative variance associated with input estimate x_i	
$[u_c(y)/ y]^2$		Relative combined variance	Relative combined variance associated with output estimate <i>y</i>	
$u(x_i,x_j))/ x_i x_j $		Estimated relative covariance	Estimated relative covariance associated with input estimates x_i and x_j	

1.1.1 Uncertainty

ITTC	Computer	Name	Definition or	SI-
Symbol	Symbol	Name	Explanation	Unit
_				
U		Expanded uncertainty	Expanded uncertainty of output estimate y that defines an interval $Y = y \pm U$ having a high level of confidence, equal to coverage factor k times the combined standard uncertainty $u_c(y)$ of y : $U = k u_c(y)$	
U_p		Expanded uncertainty associated to confidence level <i>p</i>	Expanded uncertainty of output estimate y that defines an interval $Y = y \pm U_p$ having a high level of confidence p , equal to coverage factor k_p times the combined standard uncertainty $u_c(y)$ of y : $U_p = k_p u_c(y)$	
x_i		Estimate of input quantity X_i	Estimate of input quantity X_i NOTE when x_i is determined from the arithmetic mean or av- erage of n independent repeated observation $x_i = \overline{X_i}$ $x_i = \overline{X_i}$	
X_i		i th input quantity	i th input quantity on which measurand Y depends NOTE X_i may be the physical quantity or the random variable	
$\overline{X_i}$		Estimate of the value of input quantity X_i	Estimate of the value of input quantity X_i equal to the arithmetic mean or average of n independent repeated observation $X_{i,k}$ of X_i	
$X_{i,k}$		k th independent repeated observation of X_i		
у		Estimated of measurand <i>Y</i> or Result of a measurement or Output estimate		
y_i		Estimate of measurand Y_i	Estimate of measurand Y_i when two or more measurands are determined in the same measurement	
Y		A measurand. Estimated relative uncertainty of standard uncertainty $u(x_i)$ of inputs estimate x_i		
μ_p		Expectation or mean of the probability distribution	Expectation or mean of the probability distribution of random- varying quantity <i>q</i>	
v		Degrees of freedom (general)		
v_i		Degrees of freedom	Degrees of freedom, or effective degrees of freedom of standard	

1.1.1 Uncertainty

Version 2021 1.1.1 U

ITTC	Computer	Name	Definition or	SI-
Symbol	Symbol	Name	Explanation	Unit
			uncertainty $u(x_i)$ of input estimate x_i	
$v_{\it eff}$		Effective degrees of freedom	Effective degrees of freedom of $u_c(y)$ used to obtain $t_p(v_{eff})$ for calculating expanded uncertainty U_p	
σ^2		Variance of a probability	Variance of a probability distribution of (for example) a randomly-variing quantity q , estimated by $s^2(q_k)$	
σ		Standard deviation of a probability distribution	Standard deviation of a probability distribution, equal to the positive square root of σ^2	
$\sigma^2ig(ar qig)$		Variance of q q	Variance of \overline{q} , equal to σ^2/n , estimated by $s^2(\overline{q}) = \frac{s^2(\overline{q_k})}{n}$ $s^2(\overline{q}) = \frac{s^2(q_k)}{n}$	
$\sigma(q)$		Standard deviation of \P	Standard deviation of \overline{q} , equal to the positive root of $\sigma^2(\overline{q})$	
$\sigma^2 \left[s\left(\overline{q}\right) \right]$		Variance of experimental standard deviation $s(q)$ $s(q)$ of q		
$\sigma[s(\overline{q})]$		Standard deviation of experimental standard deviation σ of σ , equal to the positive square root of $\sigma^2 \left[s(\overline{q}) \right]$		

1.1.2 Coordinates and Space Related Quantities

Orientation of coordinates

A problem of general interest, the orientation of the axes of coordinate systems, has been treated extensively in the Report of the 17th ITTC Information Committee. The present QS Group recommends that the orientations of the coordinate systems chosen for convenience should be stated explicitly in any case. The coordinate system orientation should not be inferred from the symbols and/or names of the concepts or from national or professional traditions. All sign conventions of related Quantities should be consistent with the orientation chosen.

For ready reference the recommendation of the 17th ITTC Information Committee is quoted in the following.

"In order to adapt ITTC nomenclature to common practice a proposal for a standard coordinate system was published in the newsletter No 7, March 1983, to generate discussion. The response was quite diverse. On the one hand it was suggested that instead of the two orthogonal right handed systems with the positive x-axis forward and the positive z-axis either up- or downward as proposed only one system should be selected, in particular the one with the positive z-axis upwards. On the other hand the attention of the Information Committee was drawn to the fact that in ship flow calculations neither of the two systems proposed is customary. Normally the x-axis is directed in the main flow direction, i.e. backwards, the yaxis is taken positive to starboard and the z-axis is positive upwards. The origin of the co-ordinates in this case is usually in the undisturbed free surface half way between fore and aft perpendicular.

In view of this state of affairs the Information Committee (now Quality System Group - QSG) may offer the following recommendation, if any:

Axes, coordinates

Preferably, orthogonal right handed systems of Cartesian co-ordinates should be used, orientation and origin in any particular case should be chosen for convenience.

Body axes (x,y,z)

Coordinate systems fixed in bodies, ocean platforms, or ships.

For the definition of hull forms and ocean wave properties and the analysis of structural deflections it is customary to take the *x*-axis positive forward and parallel to the reference or base line used to describe the body's shape, the *y*-axis positive to port, and the *z*-axis positive upwards.

For seakeeping and manoeuvrability problems the coordinate system is defined as follows: usually the x-axis as before the y-axis positive to starboard, and the z-axis positive downwards, the origin customarily at the centre of mass of the vehicle or at a geometrically defined position.

For ship flow calculations usually the x-axis positive in the main flow direction, i.e. backwards, the y-axis positive to starboard, and the z-axis positive upwards, the origin customarily at the intersection of the plane of the undisturbed free-surface, the centre plane, and the midship section.

Fixed or space axes (x_0,y_0,z_0)

Coordinate systems fixed in relation to the earth or the water. For further references see ISO Standard 1151/1 ...6: Terms and symbols for flight dynamics.

There may be other coordinate systems in use and there is no possibility for the adoption of a single system for all purposes. Any problem requires an adequate coordinate system and transformations between systems are simple, provided that orientations and origins are completely and correctly documented for any particular case."

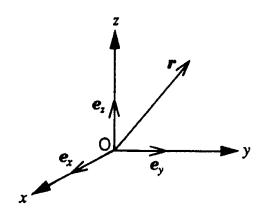
Origins of coordinates

In seakeeping and manoeuvrability problems customarily the centre of mass of the vehicle is chosen as the origin of the coordinates. This is in most cases not necessarily advantageous, as all the hydrodynamic properties entering the problems are related rather to the geometries of the bodies under investigation. So any geometrically defined point may be more adequate for the purposes at hand.

1.1.2 Coordinates and Space related Quantities 10

Item No.	Coordinates	Position vector and its differential	Name of coordinate system	Remarks
11-12.1 (-)	x, y, z	$r = xe_x + ye_y + ze_z$ $dr = dx e_x + dy e_y + dz e_z$	cartesian coordinates	e_x , e_y and e_z form an orthonormal right-handed system. See Figure 1.
11-12.2 (-)	ρ, φ, z	$\mathbf{r} = \rho \mathbf{e}_{\rho} + z \mathbf{e}_{z}$ $d\mathbf{r} = d\rho \ \mathbf{e}_{\rho} + d\varphi \ \mathbf{e}_{\varphi} + dz \ \mathbf{e}_{z}$	cylindrical coordinates	$e_{\rho}(\varphi)$, $e_{\varphi}(\varphi)$ and e_z form an orthonormal right-handed system. See Figures 2 and 3. If $z=0$, then ρ and φ are the polar coordinates
11-12.3	r, θ, φ	$r=re_r;$ $dr = dr e_r + r d \mathcal{G} e_{\mathcal{G}} + r \sin \mathcal{G} d\varphi e_{\varphi}$	spherical coordinates	$e_r(9, gyp)$, $e_g(9, \varphi)$ and $e_{\varphi}(\varphi)$ form an orthonormal right-handed system. See Figures 2 and 4.

NOTE 1 If, exceptionally, a left-handed system is used for certain purposes, this shall be clearly stated to avoid the risk of sign errors.



The x-axis is pointing towards the viewer.



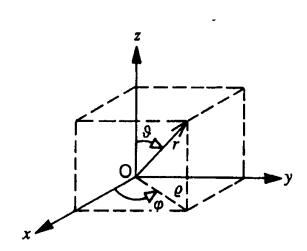


Figure 2 – Oxyz is a right-handed coordinate system

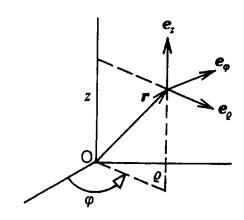


Figure 3 – Right-handed cylindrical coordinates

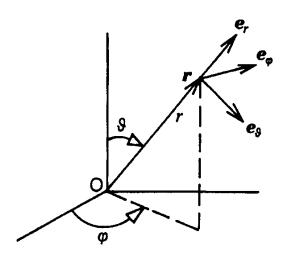


Figure 4 – Right-handed spherical coordinates

1.1 Fundamental Concepts 1.1.2 Coordinates and Space related Quantities 12

ITTC	Computer	N	Definition or	SI-
Symbol	Symbol	Name	Explanation	Unit

1.1.2.1 Basic Quantities

S	S	Any scalar quantity distributed, maybe singularly, in space	ſds	
$S^{0}{}_{ij}$	SM0(I,J)	Zero th order moment of a scalar quantity	$\int \delta_{ij} ds = \delta_{ij} S$	
S^1_{ij}	SM1(I,J)	First order moment of a scalar quantity, formerly static moments of a scalar distribution	$\int_{\mathcal{E}_{ikj}} x_k ds$	
S^2_{ij}	SM2(I,J)	Second moment of a scalar quantity, formerly moments of inertia of a scalar distribution	$\int \varepsilon_{kli} x_l \varepsilon_{jkm} x_m ds$	
S_{uv}	S(U,V)	Generalized moment of a scalar quantity distributed in space	$S_{ij} = S^{0}_{ij}$ $S_{i, 3+j} = S^{1}_{ij}^{T}$ $S_{3+i, j} = S^{1}_{ij}$ $S_{3+i, 3+j} = S^{2}_{ij}$	
T_{ij}	T(I,J)	Tensor in space referred to an orthogonal system of Cartesian coordinates fixed in the body	$T_{ij}^{\ \ s}+T_{ij}^{\ \ a}$	
$T_{ij}{}^{ m A}$	TAS(I,J)	Anti-symmetric part of a tensor	$(T_{ij} - T_{ji})/2$	
$ \begin{array}{c} T_{ij}^{\text{A}} \\ T_{ij}^{\text{S}} \\ T_{ij}^{\text{T}} \end{array} $	TSY(I,J)	Symmetric part of a tensor	$(T_{ij}+T_{ji})/2$	
T_{ij}^{T}	TTR(I,J)	Transposed tensor	T_{ji}	
$T_{ij} v_j$		Tensor product	$\Sigma T_{ij} v_j$	
u_i, v_i	U(I), V(I)	Any vector quantities	7 /	
$u_i v_i$	UVPS	Scalar product	$u_i v_i$	
$u_i v_j$	UVPD(I,J)	Diadic product	$u_i v_i$	
u×v	UVPV(I)	Vector product	$\varepsilon_{ijk}u_jv_k$	
V^0_i , V_i	V0(I),V(I)	Zeroth order moments of a vec- tor quantity distributed in space, referred to an orthogonal system of Cartesian coordinates fixed in the body	<i>sdv</i> _i	
$V^1{}_i$	V1(I)	First order moments of a vector distribution	$\int_{\mathcal{E}_{ijk}X_j}dv_k$	
V_u	V(U)	Generalized vector	$V_i = V_i^0$ $V_{3+i} = V_i^1$	
x, x_1 y, x_2 z, x_3	X, X(1) Y, X(2) Z, X(3)	Body axes and corresponding Cartesian coordinates	Right-hand orthogonal system of coordinates fixed in the body	m
x_0, x_{01} y_0, x_{02} z_0, x_{03}	X0, X0(1) Y0, X0(2) Z0, X0(3)	Space axes and corresponding Cartesian coordinates	Right-hand orthogonal system of coordinates fixed in relation to the space	m
<i>x</i> _F , <i>x</i> _{F1} <i>y</i> _F , <i>x</i> _{F2} <i>z</i> _F , <i>x</i> _{F3}	XF, XF(1) YF, XF(2) ZF, XF(3)	Flow axes and corresponding Cartesian coordinates	Right-hand orthogonal system of coordinates fixed in relation to the flow	m
$arepsilon_{ijk}$	EPS(I,J,K)	Epsilon operator	+1: ijk = 123, 231, 312 1: ijk = 321, 213, 132 0: if otherwise	
δ_{ij}	DEL(I,J)	Delta operator	+1 : <i>ij</i> = 11, 22, 33 0 : if otherwise	
			-	

1.1.3 Time and Frequency Domain Quantities

-				
ITTC	Computer	N	Definition or	SI-
Symbol	Symbol	Name	Explanation	Unit

1.1.3 Time and Frequency Domain Quantities

1.1.3.1 Basic Quantities

а	ADMP	Damping	<i>s</i> ^r , in Laplace variable	1/s
f	FR	Frequency		Hz
f _C	FC	Basic frequency in repeating functions	1 / T _C	Hz
$f_{ m S}$	FS	Frequency of sampling	$1/T_{\rm S}$ period in repeating spectra	Hz
i	I	Imaginary unit	sqrt(-1)	1
I	IM	Imaginary variable		1
j	J	Integer values	-∞+∞	1
R	R	Complex variable	$\exp(s T_S)$ Laurent transform	
S	S	Complex variable	$a + 2\pi i f$ Laplace transform	1/s
t	TI	Time	-∞ +∞	S
t_i	TI(J)	Sample time instances	j T _S	
$T_{\rm C}$	TC	Period of cycle	$1/f_{\rm C}$ duration of cycles in periodic, repeating processes	S
T_{S}	TS	Period of sampling	Duration between samples	S
X	X	Values of real quantities	x(t)	
X		Real "valued" function		
x_j	X(J)	Variables for samples values of real quantities	$x(t_j) = \int x(t)\delta(t-t_j)dt$	
Z	Z	Complex variable		

1.1.3 Time and Frequency Domain Quantities

ITTC	Computer	Nama	Definition or	SI-
Symbol	Symbol	Name	Explanation	Unit

1.1.3.2 Complex Transforms

x^{A}	XA	Analytic function	$X^{A}(t) = X(t) + iX^{H}(t)$
x^{DF}	XDF	Fourier transform of sampled	$X^{\mathrm{DF}}(f) = \Sigma x_{j} exp(-i2\pi fj T_{\mathrm{S}})$
		function	i.e. periodically repeating
			$= X(0)/2 + f_S \Sigma X^F (f + jf_S)$
			sample theorem: aliasing!
x^{DL}	XDL	Laurent transform of	$X^{\mathrm{DL}}(s) = \Sigma x_{j} \exp(-sjT_{\mathrm{S}})$
		sampled function	
x^{F}	XFT	Fourier transform	$X^{\mathrm{F}}(f) = \int X(t) \exp(-i2\pi f t) dt$
			inverse form:
			$= \int X^{F}(f) \exp(-i2\pi f t) dt$
			if $X(t) = 0$ and $a = 0$ then
			$X^{\mathrm{F}}(f) = X^{\mathrm{L}}(f)$
x^{F}_{j}	XFT(J)	Fourier transform of	$1/T_{\rm C}/X(t)\exp(-i2\pi jt/T_{\rm C})dt$
		periodic function	$t=0T_{\rm C}$
			$X^{\rm F} = \Sigma x^{\rm F}{}_{j}\delta(f - j/T_{\rm C})$
			inverse form:
			$X(t) = \Sigma x^{F} \exp(-i2\pi f j T_{C})$
x^{H}	XHT	Hilbert transform	$X^{\rm H}(t) = 1/\pi \int X(\tau)/(t-\tau)d\tau$
x^{HF}	XHF	Fourier transform of	$X^{HF}(f) = X^{F}(f)(-i \operatorname{sgn} f)$
		Hilbert transform	$(1/t)^{\mathrm{F}} = -i \operatorname{sgn} f$
x^{L}	XLT	Laplace transform	$X^{L}(s) = \int X(t) \exp(-st) dt$
			if $X(t<0) = 0$ then
			$= (X(t)\exp(-at))^F$
x^{R}	XRT	Laurent transform	$X^{R}(r) = \Sigma x_{j} r^{-j} = X^{DL}$
x^{S}	XS	Single-sided complex spectra	$X^{S}(f) = X^{F}(f)(1 + \operatorname{sgn} f)$
			$=X^{AF}$
			i.e. = $0 \text{ for } f < 0$
x^{S}_{j}	XS(J)	Single-sided complex Fourier se-	$X^{\mathrm{F}}_{j}(1+\mathrm{sgn}j)$
		ries	line spectra

1.1.3.3 Complex Quantities

z^a	ZAM	Amplitude	$mod(z) = sqrt(z^{r2} + z^{i2})$	
z^{c}	ZRE	Real or cosine component	$z^{c} = real(z) = z^{a}cos(z^{p})$	
z^i	ZIM	Imaginary or sine component	$imag(z) = z^{a}sin(z^{p}) = z^{s}$	
z^{j}	ZCJ	Conjugate	z^r - iz^i	
z^l	ZLG	(Phase) Lag		
z^p	ZPH	Phase	$\operatorname{arc}(z) = \operatorname{arctg}(z^i / z^r)$	
z^{r}	ZRE	Real or cosine component	$real(z) = z^{a}cos(z^{p}) = z^{c}$	
z^s	ZIM	Imaginary or sine component	$z^{s} = imag(z) = z^{a}sin(z^{p})$	

1.1.4 Stochastic Processes

ITTC	Computer	Nama	Definition or	SI-
Symbol	Symbol	Name	Explanation	Unit

1.1.4 Random Quantities and Stochastic Processes1.1.4.1 Random Quantities

	om Quantities			
g^{E} , g^{M} , g^{MR}	<i>G</i> MR	Expected value of a function of a random quantity	$E(g) = \int g(x)f_x(x)dx$ $x = -\infty \dots \infty$	
<i>x</i> , <i>y</i>	<i>X</i> , <i>Y</i>	Random quantities	$x(\zeta), y(\zeta)$	
x_i, y_i	X(I), Y(I)	Samples of random quantities	i = 1n	
$(x^m)^E$	<i>X</i> mMR	m-th moment of a random quantity	$(x^m)^E$	
$x^{\mathrm{D}}, x^{\mathrm{DR}}, \sigma_x$	<i>X</i> DR	Standard deviation of a random quantity	<i>x</i> ^{VR ½}	
x^{DS} , s_x	XDS	Sample deviation of a random quantity	x ^{VS 1/2} , unbiased random estimate of the standard deviation	
xx^{R}, xx^{MR}, R_{xx}	XXMR	Auto-correlation of a random quantity	$x x^{E}$	
$xy^{\mathrm{R}}, xy^{\mathrm{MR}}, R_{xy}$	XYMR	Cross-correlation of two random quantities	$x y^{\mathrm{E}}$	
x^{E} , x^{M} , x^{MR} , μ_x	<i>X</i> MR	Expectation or population mean of a random quantity	E(x)	
$x^{\rm A}, x^{\rm MS}, m_x$	XMS	Average or sample mean of a random quantity	$1/n \sum x_i$, $i = 1n$ unbiased random estimate of the expectation with $x^{AE} = x^E$ $x^{VSE} = x^V/n$ $d F_x/dx$	
x^{PD}, f_x	XPD	Probability density of a random quantity	dF_x/dx	
xy^{PD}, f_{xy}	XYPD	Joint probability density of two random quantities	$\partial F_{xy}/(\partial x \partial y)$	
x^{PF}, F_x	XPF	Probability function (distribution) of a random quantity		1
xy^{PF}, F_{xy}	XYPF	Joint probability function (distribution) function of two random quantities		1
x^{V} , x^{VR} , xx^{VR}	XVR, XXVR	Variance of a random quantity	$x^{2E} - x^{E2}$	
x^{VS} , xx^{VS}	XVS, XXVS	Sample variance of a random quantity	$1/(n-1) \Sigma (x_i - x^A)^2$ i = 1n unbiased random estimate of the variance $x^{VSE} = x^V$	
xy^{V}, xy^{VR}	XYVR	Variance of two random quantities	$x y^E - x^E y^E$	
ζ		Outcome of a random "experiment"		

1.1.4.2 Stochastic Processes

g^{MR}	GMR	Mean of a function of a random	$M(g(t)) = \lim_{t \to \infty} (1/T \int g(t)dt)$
		quantity	$t = -T/2 \dots + T/2$
			$T = -\infty \dots + \infty$
g^{MS}	GMS	Average or sample mean of a	$A(g(t)) = 1/T \int g(t)dt$
		function of a random quantity	$t = 0 \dots + T$
<i>x</i> , <i>y</i>	<i>X</i> , <i>Y</i>	Stationary stochastic process	$x(\zeta,t), y(\zeta,t)$
xx^{C} , xx^{CR} , C_{xx}	<i>XX</i> CR	Auto-covariance of a stationary	$(x(t) - x^{E})(x(t + \tau) - x^{E})^{E}$
		stochastic process	

1.1.4 Stochastic Processes

ITTC Symbol	Computer	Name	Definition or	SI- Unit
Symbol	Symbol		Explanation	Omi
$xy^{\rm C}, xy^{\rm CR}, C_{xy}$	XYCR	Cross-covariance of two stationary stochastic processes	$(x(t) - x^{\mathrm{E}})(y(t+\tau) - y^{\mathrm{E}})^{\mathrm{E}}$	
xx^{R} , xx^{RR} , R_{xx}	<i>XX</i> RR	Auto-correlation of a stationary stochastic process	$x(t)x(t+\tau)^{E} = R_{xx}(\tau)$ $R_{xx}(\tau) = R_{xx}(-\tau)$ if x is ergodic: $R_{xx}(\tau) = x(t)x(t+\tau)^{MR}$ $R_{xx}(\tau) = \int S_{xx}(\omega)\cos(\omega\tau)d\tau$ $\tau = 0 \dots \infty$	
xy^R , R_{xy}	XYRR	Cross-correlation of two stationary stochastic processes	$x(t)y(t+\tau)^{E} = R_{xy}(\tau)$ $R_{yx}(\tau) = R_{xy}(-\tau)$ if x , y are ergodic: $R_{xy}(\tau) = x(t)y(t+\tau)^{MR}$ xx^{RRSR}	
xx^{S} , S_{xx}	<i>XX</i> SR	Power spectrum or autospectral power density of a stochastic process	xx ^{RRSR}	
xy^{S}, S_{xy}	XYSR	Cross-power spectrum of two stationary stochastic processes	xy^{RRSR}	
τ	TICV	Covariance or correlation time		S
ζ		Outcome of a random "experiment"		

1.1.4.3 Probability Operators (Superscripts)

A, MS	MS	Average, sample mean
C, CR	CR	Population covariance
CS	CS	Sample covariance
D, DR	DR	Population deviation
DS	DS	Sample deviation
E, M, MR	MR	Expectation, population mean
PD	PD	Probability density
PF	PF	Probability function
S	SR	(Power) Spectrum
SS	SS	Sample spectrum
R, RR	RR	Population correlation
RS	RS	Sample correlation
V, VR	VR	Population variance
VS	VS	Sample variance

ITTC Symbols

1 Mechanics in General

1.1 Fundamental Concepts

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1.1.5	Balances and System Related Concepts	
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ITTC	Computer	Nome	Definition or	SI-
Symbol	Symbol	Name	Explanation	Unit

1.1.5 Balances and System Related Concepts

q	QQ	Quantity of the quality under consideration stored in a control volume		Q ^U
Q		Quality under consideration		Q ^U /s
Q^{C}	QCF	Convective flux		Q ^U /s
Q^{D}	QDF	Diffusive flux		Q^{U}/s
Q^{F}	QFL	Total flux across the surface of the control volume	Inward positive!	Q ^U /s
Q^{M}		Molecular diffusion		Q^{U}/s
Q^{P}	QPN	Production of sources in the control volume		Q ^U /s
Q ^S	QRT	Storage in the control volume, rate of change of the quantity stored	dq / dt	$ m Q^U/s$
Q^{T}	QDT	Turbulent diffusion		Q ^U /s

1.2.1	Inertial and	Hydrodynamic Properties	
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ITTC	Computer	Nama	Definition or	SI-
Symbol	Symbol	Name	Explanation	Unit

1.2 Solid Body Mechanics1.2.1 Inertial and Hydrodynamic Properties1.2.1.1 Basic Quantities

		Added mass coefficient in <i>i</i> th		1
A_{ij}	AM(I,J)	mode due to jth motion		
B_{ij}	DA(I,J)	Damping coefficient in <i>i</i> th mode due to <i>j</i> th motion		
C_{ij}	RF(I,J)	Restoring force coefficient in <i>i</i> th mode due to <i>j</i> th motion		
$D^{ m h}_{\ uv}$	DH(U,V)	Generalized hydrodynamic damping	$\partial F_u^h / \partial V_v$	
F_{u}^{h}	FH(U)	Generalized hydrodynamic force		
$I^{ m h}_{}$	IH(U,V)	Generalized hydrodynamic inertia	$\partial F_u^h / \partial \dot{\mathbf{V}}_v$	
$I_{ m L}$	IL	Longitudinal second moment of water-plane area	About transverse axis through centre of floatation	m ⁴
I_{T}	IT	Transverse second moment of water-plane area	About longitudinal axis through centre of floatation	m ⁴
I_y , I_{yy} , m^2_{22} , m_{55}	IY, IYY, M2(2,2), MA(5,5)	Pitch moment of inertia around the principal axis y		kg m²
I_z , I_{zz} , m^2_{33} , m_{66}	IZ, IZZ, M2(3,3), MA(6,6)	Yaw moment of inertia around the principal axis z		kg m ²
I_{xy} , I_{12} I_{yz} , I_{23} I_{zx} , I_{31}	IXY, I2(1,2) IYZ, I2(2,3) IZX, I2(3,1)	Real products of inertia in case of non-principal axes		kg m²
k_x , k_{xx}	RDGX	Roll radius of gyration around the principal axis <i>x</i>	$(I_{xx}/m)^{1/2}$	m
k_y , k_{yy}	RDGY	Pitch radius of gyration around the principal axis y	$(I_{yy}/m)^{1/2}$	m
k_z , k_{zz}	RDGZ	Yaw radius of gyration around the principal axis z	$(I_{zz}/m)^{1/2}$	m
m	MA	mass		kg
m^0_{ij} , m_{ij}	M0(I,J), MA(I,J)	Zero- th moments of mass, i.e. inertia distribution, mass tensor	$m_{ij}=m\ \delta_{ij}$	kg
m^1_{ij}	M1(I,J)	First moments of mass, i.e. inertia distribution	Alias static moments of mass	kg m
m^2_{ij} , I_{ij}	M2(I,J), IN(I,J)	Second moments of mass, i.e. inertia distribution	Alias mass moments of inertia	kg m ²
M_{uv}	MA(U,V)	Generalized mass, i. e. generalized inertia tensor of a (rigid) body referred to a body fixed coordinate system	$M_{ij} = M^0_{ij}$ $M_{i, 3+j} = M^{1T}_{ij}$ $M_{3+i, j} = M^1_{ij}$ $M_{3+i, 3+j} = M^2_{ij}$	

-		T 1	
•	,,	Loads	

ITTC	Computer	N	Definition or	SI-
Symbol	Symbol	name	Explanation	Unit

1.2.2 Loads

1.2.2.1 External Loads

F_u	F(U)	Force, generalized, load, in body coordinates	$M^{F}_{u} = M^{M}_{u}$ $F_{i} = F^{0}_{i}$ $F_{3+i} = F^{1}_{i}$	N
g_u	G(U)	Gravity field strength, generalized, in body coordinates	$g_i = g^1_i$ $g_{3+i} = 0$	m/s ²
g_i	G1(I)	Gravity field strength, in body coordinates!		m/s^2
$K, M_x,$ F^1_1, F_4 $M, M_y,$	K, M(1), F1(1), F(4)	Moment around body axis x		Nm
M , M_y , F^1_2 , F_5	M, M(2), F1(2), F(5)	Moment around body axis y		Nm
N, M_z , FN^1_3 , F_6	N, M(3), F1(3), F(6)	Moment around body axis z		Nm
$X, F_x,$ F^0_1, F_1	X, FX, F0(1), F(1)	Force in direction of body axis x		Nm
$Y, F_y,$ F^0_2, F_2	Y, FY, F0(2), F(2)	Force in direction of body axis y		Nm
$Z, F_z,$ F^0_3, F_3	Z, FZ, F0(3), F(3)	Force in direction of body axis z		Nm
G_u	G(U)	Gravity or weight force, generalized, in body co-ordinates!	$G_u = m_{uv} g_v$	N
G^0i , G_i	G0(I)	Gravity or weight force in body coordinates!	$G_i = G^0{}_i = m^0{}_{ij} g_j$ $= mg_i$	N
G^1_i	G1(I)	Gravity or weight moment in body coordinates!	$= mg_i$ $G_{3+i} = G^1{}_i = \varepsilon_{ikj} x_k G^0{}_j$ $= m^1{}_{ij} g_j$	Nm
q	UNQ	Load per unit length	7 0/	N/m
w	WPUL	Weight per unit length	dW/dx_1	N/m

ITTC Symbols

1 Mechanics in General

1.2 Solid Body Mechanics 1.2.2 Loads

Version 2021 1.2.2

Definition or	CI

ITTC	Computer	Nama	Definition or	SI-
Symbol	Symbol	Name	Explanation	Unit

1.2.2.2 Sectional Loads

F^{S}_{u}	FS(U)	Force or load acting at a given planar cross-section of the body, generalized, in section coordi- nates!	$F_{i}^{S} = F_{i}^{S0}$ $F_{3+i}^{S} = F_{i}^{S1} = M_{i}^{B}$	N Nm
$F^{\mathbf{S}}_{i}$	FS(I)	Shearing force	F^{80}_{2} , F^{80}_{3}	N
F^{T}	FT, FS(1)	Tensioning or normal force	F^{S0} 1	N
$M^{\mathrm{B}}{}_{i}$	MB(I)	Bending moment	F^{S1}_{2} , F^{S1}_{3}	Nm
M^{T}	MT, MB(1)	Twisting or torsional moment	F ^{S1} 1	Nm

1.2.3	Rigid	Body	Motions
1.2.0	INICIM	Doug	TITOUTIS

ITTC	Computer	N	Definition or	SI-
Symbol	Symbol	name	Explanation	Unit

1.2.3 Rigid Body Motions1.2.3.1 Motions

1.2.3.1	0110113			
\boldsymbol{L}	L	Angular momentum	$\boldsymbol{L} = I\boldsymbol{\omega} (= r^2 m v)$	Kg m s ⁻¹
P	P	Linear momentum	P = m v	Kg m s ⁻¹
p , ω_x ,	P, OMX,	Rotational velocity around body		rad/s
v^{0}_{1} , v_{4}	V0(1), V(4)	axis x		rad/s
q , ω_y ,	Q, OMY,	Rotational velocity around body		rad/s
v^{0}_{2} , v_{5}	V0(2), V(5)	axis y		rad/s
r , ω_z ,	R, OMZ,	Rotational velocity around body		rad/s
v^0_3 , v_6	V0(3), V(6)	axis z		Tau/S
u , v_x ,	U, VX,	Translatory velocity in the direc-		m/s
v^{1}_{1} , v_{1}	V1(1), V(1)	tion of body axis x		111/8
v , v_y ,	V, VY,	Translatory velocity in the direc-		m/s
v^{1}_{2} , v_{2}	V1(2), V(2)	tion of body axis y		111/8
W , V_z ,	W, VZ,	Translatory velocity in the direc-		m/s
v^{1}_{3} , v_{3}	V1(3), V(3)	tion of body axis z		111/8
		Components of generalized ve-	$v_{\cdot} \equiv v^{1}$.	m/s
v_u	V(U)	locity or motion relative to body	$v_i = v_i^1$ $v_{3+i} = v_i^0$	rad/s
		axes	V3+1 V 1	Tad/5
\dot{p}	PR	Rates of change of components		
\dot{q}	QR	of rotational velocity relative to		rad/s ²
	RR	body axes		Tad/3
<i>r</i>	Idit	oody axes		
ù	UR	Rates of change of components		
$\dot{\mathcal{V}}$	VR	of linear velocity relative to		m/s^2
\dot{w}	WR	body axes		
α	AA	Angular acceleration	$d\omega/dt$	rad/s ²
			1	<u> </u>

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ITTC	Computer	N	Definition or	SI-
Symbol	Symbol	name	Explanation	Unit

1.2.3.2 Attitudes

α	AT ALFA	Angle of attack	The angle of the longitudinal body axis from the projection into the principal plane of symmetry of the velocity of the origin of the body axes relative	rad
			to the fluid, positive in the positive sense of rotation about the y-axis	
β	DR BET	Angle of drift or side-slip	The angle to the principal plane of symmetry from the velocity vector of the origin of the body axes relative to the fluid, positive in the positive sense of rotation about the z-axis	rad
γ	RO GAMR	Projected angle of roll or heel	The angular displacement about the x_0 axis of the principal plane of symmetry from the vertical, positive in the positive sense of rotation about the x_0 axis	rad
φ	X(4) RO PHIR	Angle of roll, heel or list	Positive in the positive sense of rotation about the <i>x</i> -axis	rad
θ	X(5) TR TETP	Angle of pitch or trim	Positive in the positive sense of rotation about the <i>y</i> -axis	rad
Ψ	X(6) YA PSIY	Angle of yaw, heading or course	Positive in the positive sense of rotation about the <i>z</i> -axis	rad

1.3.1 Flow Parameters

ITTC	Computer	N	Definition or	SI-
Symbol	Symbol	Name	Explanation	Unit

1.3 Fluid Mechanics

1.3.1 Flow Parameters

1.3.1.1 Fluid Properties

С	CS	Velocity of sound	$(E / \rho)^{1/2}$	m/s
E	EL	Modulus of elasticity		Pa
w	WD	Weight density	ρg (See 1.1.1)	
κ	CK	Kinematic capillarity	σ/ρ	m^3/s^2
μ	VI	Viscosity		kg/ms
v	VK	Kinematic viscosity	μ / ρ	m^2/s
ρ	DN, RHO	Mass density		kg/m ³
σ	CA	Capillarity	Surface tension per unit length	kg/s ²

1.3.1.2 Flow parameters

1.3.1.2 110	v parameters			
Во	BN	Boussinesq number	$V/(gR_{\rm H})^{1/2}$	1
Са	CN	Cauchy number	$V/(E/\rho)^{1/2}$	1
Fr	FN	Froude number	$V/(gL)^{1/2}$	1
Fr_h	FH	Froude depth number	$V/(g h)^{1/2}$	1
Fr_{∇}	FV	Froude displacement number	$V/(g V^{1/3})^{1/2}$	1
Ма	MN	Mach number	V/c	1
Re	RN	Reynolds number	VL/v	1
Re _{0.7}	RN07	Propeller Reynolds number at 0.7 R	$Re_{0.7} = \frac{c_{0.7}\sqrt{V_A^2 + (0.7\pi nD)^2}}{v}$	1
St	SN	Strouhal number	fL/V	1
Th	TN	Thoma number, Cavitation number	$(p_A-p_V)/q$	1
We	WN	Weber number	$V^2 L / \kappa$	1

ITTC Symbols

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1 Mechanics in General

1.3 Fluid Mechanics

1.3.1 Flow Parameters

ITTC	Computer	Nama	Definition or	SI-
Symbol	Symbol	Name	Explanation	Unit

1.3.1.3 Boundary conditions

k	HK	Roughness height or magnitude	Roughness height, usually in terms of some average	m
$k_{ m s}$	SK	Sand roughness	Mean diameter of the equivalent sand grains covering a surface	m
$R_{ m H}$	RH	Hydraulic radius	Area of section divided by wet- ted perimeter	m

Version 2021 1.3.2 Flow Fields

ITTC	Computer	N	Definition or	SI-
Symbol	Symbol	name	Explanation	Unit

1.3.2 Flow Fields 1.3.2.1 Velocities etc.

e	ED	Density of total flow energy	$\rho V^2 / 2 + p + \rho g h$	Pa
f_i	FS(I)	Mass specific force	Strength of force fields, usually only gravity field g_i	m/s ²
h	HS	Static pressure head	Δz_0 , z_0 -axis positive vertical up!	m
Н	HT	Total head	e/w = h + p/w + q/w	m
p	PR, ES	Pressure, density of static flow energy		Pa
p_0	P0	Ambient pressure in undisturbed flow		Pa
q	PD, EK	Dynamic pressure, density of kinetic flow energy,	$\rho V^2/2$	Pa
Q	QF, QFLOW	Rate of flow	Volume passing across a control surface in time unit	m ³ /s
$S_{ m H}$	THL	Total head loss		m
S^{R}_{ij}	SR(I,J)	Turbulent or Reynolds stress	$\rho v_i v_j^{CR}$	Pa
S_{ij}	ST(I,J)	Total stress tensor	Density of total diffusive mo- mentum flux due to molecular and turbulent exchange	Pa
$s^{ m V}_{ij}$	SV(I,J)	Viscous stress		Pa
u, v_x, v_1 v, v_y, v_2 w, v_z, v_3	VX, V1 VY, V2 VZ, V3	Velocity component in direction of x, y, z axes		m/s
v_i	V(I)	Velocity		m/s
V	VA	Velocity	$V = v_i v_i^{1/2}$	m/s
V_0	V0	Velocity of undisturbed flow		m/s
$ au_w$	TAUW	Wall shear stress	$\mu \left(\partial U / \partial y \right)_{v=0}$	Pa

1.3.2.2 Circulation etc.

Γ^{n}	CN	Normalized circulation	$\Gamma / (\pi D V)$ $\pi \text{ is frequently omitted}$	1
I	ID	Induction factor	Ratio between velocities induced by helicoidal and by straight line vortices	1
Γ	VD	Vortex density	Strength per length or per area of vortex distribution	m/s
Γ	CC	Circulation	$\int V ds$ along a closed line	m ² /s
Φ	PO	Potential function		m^2/s
Ψ	SF	Stream function	ψ = const is the equation of a stream surface	m ³ /s

1.3.3 Lifting Surfaces Version 2021

ool		Explanation	Unit
ices			
	Projected area	here	m^2
		$U \subset M$	m
F	•		m
		A/h	m
		ATO	m
			m
			m
			m
	**		rad
			rad
	Thickness ratio of foil section	t / c	1
ТВ	of struts	$t_{\rm B}$ / $c_{\rm S}$	1
TF		f/c	1
FL	Angle of flap deflection		rad
TL	Camber ratio of lower side of	$f_{\rm L}/c$	1
TS		ts / cs	1
TT	section	$t_{\rm S} / c_{\rm STH}$	1
TU	Camber ratio of upper side	$f_{\rm U}$ / c	1
	Taper ratio	$c_{\rm t}$ / $c_{\rm r}$	1
	Aspect ratio	b^2/A	1
s etc			
	Induced velocity		m/s
	Resultant velocity of flow ap-	Taking vortex induced velocities	m/s
	promoning a my moren		
	Angle of attack or incidence		rad
A	8		
P.F.	ECC. 4' 1 - C - 44 - 1 ''		
	_	the chord line including the ef-	rad
E	dence	fect of induced velocities	
\$E	Geometric angle of attack or in-	The angle of attack relative to	
		the chord line neglecting the ef-	rad
<u> </u>	Cidence		
	Hydrodynamic angle of attack		rad
I	Try arouy number ungre or account		144
	Ideal angle of attack		rad
S	Tucar angle of attack		iau
L.			
	Angle of zero lift		rad
	F ME TP RT J SW SL TT TB TF TFL TL TS TT TU Es etc GE, GG HY, II D, SS	ME Mean chord length Tip chord length Camber of lower side (general) Camber of upper side Sweep angle Camber of upper side Sweep angle Camber of of foil section Camber of trailing edge of struts Camber ratio of trailing edge of struts Camber ratio of mean line (general) Thickness ratio of lower side of foil Camber ratio of lower side of foil Camber ratio of strut Theoretical thickness ratio of Section TU Camber ratio of upper side Taper ratio Aspect ratio Se etc Induced velocity Resultant velocity of flow approaching a hydrofoil Angle of attack or incidence EF, Effective angle of attack or incidence GE, Geometric angle of attack or incidence GE, Geometric angle of attack Ideal angle of attack D, Ideal angle of attack LL, Angle of zero lift	Wing or foil span

ITTC	Computer	Name	Definition or	SI-
Symbol	Symbol		Explanation	Unit
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1.3.3.3 Forces

$D_{ m F}$	DRF	Foil drag	Force in the direction of motion of an immersed foil	N
D_{I}	DRIND	Induced drag	For finite span foil, the component of lift in the direction of motion	N
$D_{ m INT}$	DRINT	Interference drag	Due to mutual interaction of the boundary layers of intersecting foil	N
$D_{ m P}$	DRSE	Section or profile drag at zero lift	Streamline drag	N
$L_{ m F}$	LF	Lift force on foil	$C_L A_{\rm FT} q$	N
L_0	LF0	Lift force for angle of attack of zero	$C_{L0}A_{ m FT}q$	N

1.3.3.4 Sectional coefficients

C_D	CDSE	Section drag coefficient		1
C_{DI}	CDSI	Section induced drag coefficient		1
C_L	CLSE	Section lift coefficient		1
C_{L0}	CLSE0	Section lift coefficient for angle of attack of zero		1
C_M	CMSE	Section moment coefficient		1
3	EPSLD	Lift-Drag ratio	L/D	1

1.3.4 Boundary Layers

ITTC	Computer	Nama	Definition or	SI-
Symbol	Symbol	Name	Explanation	Unit

1.3.4 Boundary Layers1.3.4.1 Two-dimensional Boundary Layers

wo-dimensional	Boundary Layers		
CFL	Skin friction coefficient	$\tau / (\rho U_e^2 / 2)$	1
CQF	Entrainment factor	$1/(U_e dQ/dx)$	1
HBL	Boundary layer shape parameter	δ^* / Θ	1
HQF	Entrainment shape parameter	$(\delta - \delta^*) / \Theta$	1
PR	Static pressure		Pa
PT	Total pressure		Pa
QF	Entrainment	$\int_{a}^{b} U dy$	m²/s
RDELS	Reynolds number based on displacement thickness	$U_{\infty}\delta^*/v$ or $U_e\delta^*/v$	1
RTHETA	mentum thickness	$U_{\infty}\Theta/v$ or $U_{e}\Theta/v$	1
UFL	ary layer		m/s
UFLS	locity fluctuations		m/s
UPLUS	Non-dimensional distance from surface	$U/u_{ au}$	1
UTAU	Shear (friction) velocity	$(\tau/\rho)^{1/2}$	m/s
UMR	Time mean of velocity in boundary layer		m/s
UIN	Instantaneous velocity		m/s
UFS	Free-stream velocity far from the surface		m/s
UE	Velocity at the edge of the boundary layer at $y=\delta_{995}$		m/s
UDEF	Velocity defect in boundary layer	$(U_{e^-}U)/u_{\tau}$	1
YPLUS	Non-dimensional distance from the wall	$y u_{\tau} / v$	1
BETE	Equilibrium parameter	$\delta^* / (\tau_w dp / dx)$	1
DEL	Thickness of a boundary layer at $U=0.995U_e$		m
DELS	Displacement thickness of boundary layer	$\int (U_{\rm e} - U) / U_{\rm e} dy$	m
K	von Karman constant	0.41	1
PRGR	Pressure gradient parameter	δ_{995} / ($v dU_e / dx$)	1
ENTH	Energy thickness	$\int (U/U_{\rm e}) (1 - U^2/U_{\rm e}^2) dy$	m
THETA	Momentum thickness	$\int (U/U_{\rm e}) (1 - U/U_{\rm e}) dy$	m
TAUW	Local skin friction	$\mu \left(\partial U / \partial y \right)_{y=0}$	Pa
	CFL CQF HBL HQF PR PT QF RDELS RTHETA UFL UFLS UPLUS UTAU UMR UIN UFS UE UDEF YPLUS BETE DEL DELS K PRGR ENTH THETA	CQF Entrainment factor HBL Boundary layer shape parameter HQF Entrainment shape parameter PR Static pressure PT Total pressure QF Entrainment RDELS Reynolds number based on displacement thickness RTHETA Reynolds number based on momentum thickness UFL Velocity fluctuations in boundary layer UFLS Root mean square value of velocity fluctuations UPLUS Non-dimensional distance from surface UTAU Shear (friction) velocity UMR Time mean of velocity in boundary layer UIN Instantaneous velocity UFS Free-stream velocity far from the surface UE Velocity at the edge of the boundary layer at y=δ995 UDEF Velocity defect in boundary layer YPLUS Non-dimensional distance from the wall BETE Equilibrium parameter DEL Displacement thickness of boundary layer at U=0.995Ue DELS Displacement thickness of boundary layer K von Karman constant PRGR Pressure gradient parameter ENTH Energ	CFL Skin friction coefficient $\tau/(\rho U_e^2/2)$ CQF Entrainment factor $1/(U_c dQ/dx)$ HBL Boundary layer shape parameter δ^*/Θ HQF Entrainment shape parameter δ^*/Θ PR Static pressure PT Total pressure QF Entrainment $\int_a^b Udy$ RDELS Reynolds number based on displacement thickness RTHETA Reynolds number based on momentum thickness UFL Velocity fluctuations in boundary layer UFLS Root mean square value of velocity fluctuations UPLUS Non-dimensional distance from surface UPLUS Non-dimensional distance from surface UIN Instantaneous velocity UFS Free-stream velocity far from the surface UE Velocity at the edge of the boundary layer at $y=\delta_{995}$ UDEF Velocity defect in boundary layer YPLUS Non-dimensional distance from the surface UE Velocity defect in boundary layer at $y=\delta_{995}$ UDEF Velocity defect in boundary layer at $y=\delta_{995}$ UDEL Displacement thickness of boundary layer at $y=\delta_{995}/V$ <t< td=""></t<>

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ITTC Symbol	Computer Symbol	Name	Definition or Explanation	SI- Unit
Symbol	Symbol		Explanation	Ollit
.3.5 Cav	itation			
	ow parameters			
$\frac{a_{\rm s}}{a_{\rm s}}$	GR	Gas content ratio	$\alpha/\alpha_{\rm S}$	1
uş			Actual amount of solved and un-	
α	GC	Gas content	dissolved gas in a liquid	ppm
α_{S}	GS	Gas content of saturated liquid	Maximum amount of gas solved in a liquid at a given temperature	ppm
σ	CNPC	Cavitation number	$(p_A - p_C) / q$	1
$\sigma_{ m I}$	CNPI	Inception cavitation number		1
$\sigma_{ m V}$	CNPV	Vapour cavitation number	$(p_{\rm A} - p_{\rm V}) / q$	1
.3.5.2 Flo	ow fields			
$D_{\rm C}$	DC	Cavity drag		N
		3 3	Stream wise dimension of a	
l_{C}	LC	Cavity length	fully-developed cavitating re-	m
			gion	
p_{A}	PA	Ambient pressure		Pa
	PACO	Callanca praegura	Absolute ambient pressure at	Pa
$p_{ m AC}$	PACO	Collapse pressure	which cavities collapse	Ра
			Absolute ambient pressure at	
$p_{ m AI}$	PAIC	Critical pressure	which cavitation inception takes	Pa
		_	place	
no	PC	Cavity pressure	Pressure within a steady or	Pa
$p_{\rm C}$	TC	Cavity pressure	quasi-steady cavity	1 a
			Pressure, may be negative, i.e.	
p_{CI}	PCIN	Initial cavity pressure	tensile strength, necessary to cre-	Pa
			ate a cavity	
$p_{ m V}$	PV	Vapour pressure of water	At a given temperature!	Pa
U_{I}	UNIN	Critical velocity	Free stream velocity at which	m/s
		,	cavitation inception takes place	
$V_{\rm L}$	VOLS	Volume loss	W _L / w	m ³
***	TI ITTE	****	Weight of material eroded from	3.7/
$W_{ m L}$	WTLS	Weight loss	a specimen during a specified	N/s
			time	
			Maximum height of a fully-de-	
$\delta_{ m C}$	HC	Cavity height or thickness	veloped cavity, normal to the	m
		, ,	surface and the stream-wise di-	
2.5.2 B			rection of the cavity	
	mps		T	
$H_{\rm N}$	HTNT	Net useful head of turbo-engines		m
$H_{ m U}$	HTUS	Total head upstream of turbo-en-		m
		gines		
Th, σ	TN	Thoma number	$(H_U - p_V/w)/H_N$	1

1.4.1 Waves

ITTC	Computer	N	Definition or	SI-
Symbol	Symbol	Name	Explanation	Unit

1.4 Environmental Mechanics

1.4.1 Waves

This section is related to Sections 3.1.2 Time and Frequency Domain Quantities and 3.1.3 Random Quantities and Stochastic Processes.

1.4.1.1 Periodic waves

1.4.1.1	reflouic waves			
CW	VP	Wave phase velocity or celerity	$L_{\rm W}/T_{\rm W} = \sqrt{gL_{\rm W}/2\pi}$ in deep water	m/s
$c_{\mathrm{W}i}$	VP(I)	Wave phase velocity of harmonic components of a periodic wave	$const = c_W$ for periodic waves in deep water	m/s
C _G	VG	Wave group velocity or celerity	The average :rate of advance of the energy in a finite train of gravity waves	m/s
$f_{ m W}$	FW	Basic wave frequency	1 / T _W	Hz
$f_{\mathrm{W}i}$	FW(I)	Frequencies of harmonic components of a periodic wave	$if_{ m W}$	Hz
$H_{ m W}$	HW	Wave height	The vertical distance from wave crest to wave trough, or twice the wave amplitude of a harmonic wave. $\eta_{\rm C}$ - $\eta_{\rm T}$	m
<i>k</i> , <i>κ</i>	WN	Wave number	$2\pi/L_{\rm W}=\omega^2/g$	1/m
$L_{ m W}$, $\lambda_{ m W}$	LW	Wave length	The horizontal distance be- tween adjacent wave crests in the direction of advance	m
$T_{ m W}$	TW	Basic wave period	Time between the passage of two successive wave crests past a fixed point. $1/f_W$	s
μ	WD	Wave direction	The angle between the direction of a component wave and the x_0 axis	rad
η	EW	Instantaneous wave elevation at a given location	z-axis positive vertical up, zero at mean water level;	m
$\eta^{lpha}{}_{i}$	EWAM(I)	Amplitudes of harmonic components of a periodic wave	$\eta^{ ext{FS}lpha}$	m
$\eta^{ extsf{p}}_{i}$, $arepsilon_{i}$	EWPH(I)	Phases of harmonic components of a periodic wave	$\eta^{ ext{FSp}}$	rad
η_{C}	EC	Wave crest elevation		m
η_{T}	ET	Wave trough depression	Negative values!	m
ζ	DW	Instantaneous wave depression	z-axis positive vertical down, zero at mean water level	m
ζ_{A}	WAMP	Wave amplitude	Radius of orbital motion of a surface wave particle	m
ω_{W} , σ	FC	Circular wave frequency	$2\pi f_{\rm W} = 2\pi/T_{\rm W}$	rad/s

1.4.1.2 Irregular waves

$H_{ m d}$	HD	Wave height by zero down- crossing	The vertical distance between a successive crest and trough.	m
$H_{ m u}$	HU	Wave height by zero up-crossing	The vertical distance between a successive trough and crest	m
$H_{1/3}$	H13	Significant wave height	Average of the highest one third wave heights	m

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1.4.1 Waves

ITTC	Computer	Name	Definition or	SI-
Symbol	Symbol		Explanation	Unit
$T_{1/3d}$	T13D	Significant wave period	By downcrossing analysis	s
$T_{1/3u}$	T13U	Significant wave period	By upcrossing analysis	S
1 1/3u	1130		Time elapsing between two suc-	3
$T_{\rm d}$	TD	Wave periods by zero down-	cessive downward crossings of	s
1 d	1D	crossing	zero in a record	3
			Time elapsing between two suc-	
$T_{ m u}$	TU	Wave periods by zero up-cross-	cessive upward crossings of zero	s
ı u		ing	in a record	5
		Maximum of elevations of wave	In a record	
$\eta_{ m C}$	EC	crests in a record		m
		Elevations of wave troughs in a		
η_T	ET	record	Negative values!	m
			The horizontal distance between	
$\lambda_{ m d}$	LD	Wave length by zero down-	adjacent down crossing in the di-	m
~		crossing	rection of advance	
			The horizontal distance between	
$\lambda_{ m u}$	LU	Wave length by zero up-crossing	adjacent up crossing in the direc-	m
			tion of advance	
.4.1.3 Tir	me Domain Ana	alysis		
		Wave height estimated from vis-		
$H_{ m WV}$	HWV	ual observation		m
		Significant wave height. Sum of	Average of the highest one third	
$H_{W1/3}$	H13	significant wave height of swell	wave heights	m
		and wind waves	wave neights	
$H_{1/3S}$	H13S	Significant wave height of swell	Average of the highest one third	m
111/38	11130		wave heights of the swell.	111
		(environmental mechanics,	Average of the highest one third	
$H_{1/3W}$	H13W	waves) Significant wave height	wave heights of the wind waves.	m
		of wind waves.		
$H_{1/3u}$	H13U	Zero up-crossing significant	Average of the highest one third	m
		wave height	zero up-crossing wave heights	
11	HWDC	Estimate of significant wave		
H_{σ}	HWDS	height from sample deviation of		m
		wave elevation record Wave length estimated by visual	Measured in the direction of	-
$L_{ m WV}$	LWV			m
		observation	wave propagation The average interval in years be-	
$T_{ m rt}$	TRT	Return period	tween times that a given design	
1 It	IKI	Return period	wave is exceeded	
$T_{\rm R}$	TR	Duration of record	$1/f_{\rm R}$	S
* N	110	2 diamon of 100014	$1/f_{\rm S}$,	
T_{S}	TS	Sample interval	time between two successive	s
- 0	1~		samples	
	TEXA IX I	Wave period estimated from vis-	F	
$T_{ m WV}$	TWV	ual observation		S

1.4.1.4 Frequency Domain Analysis

b	В	Bandwidth of spectral resolution	Sampling frequency divided by the number of transform points	Hz
$C_{\rm r}$	CRA	Average reflection coefficient		1
$C_{\rm r}(f)$	CRF	Reflection coefficient amplitude function		1
$f_{ m P}$	FRPK	Spectral peak in frequency	Frequency at which the spectrum has its maximum	Hz

1.4.1 Waves

1	1 4	1	Waves

ITTC Symbol	Computer Symbol	Name	Definition or Explanation	SI- Unit
	•		-	
f_{R}	FRRC	Frequency resolution	$1/T_{\rm R}$	Hz
f_{S}	FRSA	Sample frequency	$1/T_{\rm S}$	Hz
H_{mo}	НМО	Significant wave height based on zeroth moment for narrow banded spectrum	$4 (m_{\theta})^{1/2}$	m
H_{σ}	HWDS	Estimate of significant wave height from sample deviation of wave elevation record		m
m_n	MN	n-th moment of wave power spectral density	$\int f^n S(f)df$	m^2/s^n
$S_i(f)$, $S_i(\omega)$	EISF, EISC	Incident wave power spectral density		m ² /Hz
$S_r(f)$, $S_r(\omega)$	ERSF, ERSC	Reflected wave power spectral density		m ² /Hz
$S_{\eta}(f)$, $S_{\eta}(\omega)$	EWSF, EWSC	Wave power spectral density		m ² /Hz
T_P	TP	Period with maximum energy	$2\pi f_{\rm P}$	s
T_{01}	T1	Average period from zeroth and first moment	m_0/m_1	S
T_{02}	T2	Average period from zeroth and second moment	$(m_0/m_2)^{1/2}$	S

1.4.1.5 Directional Waves

1.1.1.5 DHC	ctional waves			
$D_{\mathrm{X}}(f, \theta), \ D_{\mathrm{X}}(\omega, \mu), \ \sigma_{\theta}$	DIRSF SIGMAOX	Directional spreading function	$\int_{0}^{2\pi} D_{X}(f,\theta) = 1$ $\int_{0}^{2\pi} D_{X}(f,\theta) d\theta = 1$	rad
f	FR	Frequency	$2\pi\omega=1/T$	Hz
$S_{\zeta}(\omega,\mu)$ $S_{\theta}(\omega,\mu)$ etc.	S2ZET S2TET etc.	Two dimensional spectral density		1
$S_{ ho}(f, \theta)$ $S_{\zeta}(\omega, \mu)$	STHETA	Directional spectral density		m²/Hz/ rad
θ , μ	CWD	Component wave direction		rad
$ heta_{ m m}$	MWD THETAMOX	Mean or dominant wave direction		rad

ITTC	Computer	Nome	Definition or	SI-
Symbol	Symbol	Name	Explanation	Unit

1.4.2 Wind

1.4.2.1 Basic Quantities

C_{10}	C10M	Surface drag coefficient	$(0.08 + 0.065U_{10})10^{-3}$	
F	FETCH	Fetch length	Distance over water the wind blows	m
$t_{ m d}$	DURATN	Wind duration		S
T_{rt}	TRT	Return period	The average interval in years be- tween times that a given wind speed is exceeded	
u_z , u_{zi}	UFLUCT	Turbulent wind fluctuations		m/s
U_A , $u*$	USHEAR	Wind shear velocity	$C_{10}^{1/2} U_{10}$ or $0.71 U_{10}^{1.23}$	m/s
U_{10}	U10M	Reference mean wind speed at elevation 10 meters above sea surface	$U_{10} = (10/z)^{1/7} \ U_z^A$	m/s
$U_z{}^{ m A}$	UZA	Average wind speed at elevation z above the sea surface	$(U_z + u_{zi})^A$ $U_z^A = (z/10)^{1/7} U_{10} \text{ or }$ $U_z^A = U_{10} + U_A \ln(z/10)$	m/s
$V_{ m WR}$	VWREL	Apparent wind velocity	see section 1.4.1	m/s
$V_{ m WT}$	VWABS	True wind velocity	see section 1.4.1	m/s
X_{F}	FDIM	Dimensionless Fetch	gF/U_{10}^{2}	
Z	ZSURF	Height above the sea surface in meters		m
$eta_{ m WA}$	BETWA	Apparent wind angle (relative to vessel course)	see section 2.6	rad
$eta_{ m WT}$	BETWT	True wind angle (relative to vessel course)	see section 2.6	rad
$ heta_{ m W}$	TETWI	Wind direction		rad

1.4.5	ice Micchanics	

ITTC	Computer	Nama	Definition or	SI-
Symbol	Symbol	Name	Explanation	Unit

1.4.3 Ice Mechanics

1.4.3.1 Basic Quantities

E_{I}	MEI	Modulus of elasticity of ice		Pa
$S_{\rm I}$	SAIC	Salinity of ice	Weight of salt per unit weight of ice	1
$S_{ m W}$	SAWA	Salinity of water	Weight of dissolved salt per unit weight of saline water	1
t_{A}	TEAI	Temperature of air		°C
$t_{ m I}$	TEIC	Local temperature of ice		°C
$t_{ m W}$	TEWA	Temperature of water		°C
$\delta_{ m I}$	ELIC	Deflection of ice sheet	Vertical elevation of ice surface	m
$arepsilon_{ m I}$	STIC	Ice strain	Elongation per unit length	1
$\dot{\mathcal{E}}_{ m I}$	STRTIC	Ice strain rate	$\partial \varepsilon / \partial \tau$	1/s
$\mu_{\rm I}$	POIIC	Poisson's ratio of ice		1
$v_{\rm A}$	POAI	Relative volume of air	Volume of gas pores per unit volume of ice	1
$v_{ m B}$	POBR	Relative volume of brine	Volume of liquid phase per unit volume of ice	1
v_0	POIC	Total porosity of ice	$v_0 = v_A + v_B$	1
$ ho_{ m I}$	DNIC	Mass density of ice	Mass of ice per unit volume	kg/m ³
$ ho_{ m SN}$	DNSN	Mass density of snow	Mass of snow per unit volume	kg/m ³
$ ho_{ m W}$	DNWA	Mass density of water		kg/m ³
$ ho_{\!\scriptscriptstyle arDella}$	DNWI	Density difference	$ ho_{arDelta}= ho_W$ - $ ho_I$	kg/m ³
$\sigma_{ m CI}$	SCIC	Compressive strength of ice		Pa
$\sigma_{ m FI}$	SFIC	Flexural strength of ice		Pa
$\sigma_{ m TI}$	SNIC	Tensile strength of ice		Pa
$ au_{ m SI}$	STIC	Shear strength of ice		Pa

1 **Mechanics in General**

1.5 Noise 1.5.1 Underwater noise Version 2021

ITTC	Computer	Name	Definition or	SI-
Symbol	Symbol	Name	Explanation	Unit

1.5 Noise

1.5.1 Underwater Noise

d	DIDR	Distance hydrophone to acoustic centre		m
L_p	SPL	Sound pressure level	$L_p = 10 \log_{10} \left(\frac{\bar{p}_{rms}^2}{p_{ref}^2} \right) \text{dB, } p_{ref}$ $= 1 \mu \text{Pa}$	
$L_{ m S}$	SRNL	Underwater sound radiated noise level at a reference distance of 1m	$\begin{aligned} L_{s} &= L_{p} \\ &+ 20 \log_{10} \left[\frac{d}{d_{ref}} \right] \text{dB, } d_{ref} = 1 \text{ m} \end{aligned}$	
p	SPRE	Sound pressure		Pa

2.1 Basic Quantities

ITTC	Computer	N	Definition or	SI-
Symbol	Symbol	Name	Explanation	Unit

2. SHIPS IN GENERAL

2.1 Basic Quantities

	c Quantities			,
a, a^1	AC, A1	Linear or translatory acceleration	dv / dt	m/s^2
A	A, AR, AREA	Area in general		m^2
В	B, BR	Breadth		m
C, F^{F_2}	FF(2)	Cross force	Force normal to lift and drag (forces)	N
Сс	CC	Cross force coefficient	$C_{\rm C} = \frac{C}{qA}$	1
D, F^{F_1}	FF(1)	Resistance, Drag (force)	Force opposing translatory velocity, generally for a completely immersed body	N
d, D	D, DI	Diameter		m
E	E, EN	Energy		J
f	FR	Frequency	1/T	Hz
F, F^0	F, F0	Force		N
g	G, GR	Acceleration of gravity	Weight force / mass, strength of the earth gravity field	m/s ²
h	DE	Depth		m
Н	H, HT	Height		m
I	I, IN	Moment of inertia	Second order moment of a mass distribution	kg m ²
L	L, LE	Length		m
L, F^F_3	FF(3)	Lift (force)	Force perpendicular to translatory velocity	N
m	M, MA, MASS	Mass		kg
M, F^1	M1, F1	Moment of forces	First order moment of a force distri- bution	Nm
\overline{M}	MO	Momentum		Ns
n, N	FR, N	Frequency or rate of revolution	Alias RPS (RPM in some propulsor applications)	Hz
\overline{P}	P, PO	Power		W
r, R	RD	Radius		m
R, F^F_1	R, RE, FF(1)	Resistance (force)	Force opposing translatory velocity	N
S	SP	Distance along path		m
t	TI	Time		s
t	TE	Temperature		K
T	TC	Period	Duration of a cycle of a repeating or periodic, not necessarily harmonic process	s
\overline{U}	U, UN	Undisturbed velocity of a fluid		m/s
v, V ¹	V, V1	Linear or translatory velocity of a body	ds / dt	m/s
V	VO	Volume		m^3
w	WD	Weight density, formerly specific weight	$dW/dV = \rho g$	N/m³
W	WT	Weight (force), gravity force acting on a body		N
γ	MR	Relative mass or weight, in English speaking countries called specific gravity	Mass density of a substance divided by mass density of distilled water at 4°C	1
	EF, ETA	Efficiency	Ratio of powers	

2.1 Basic Quantities

ITTC	Computer	Name -	Definition or	SI-
Symbol	Symbol	Name	Explanation	Unit
ρ	DN, RHO	Mass density	dm / dV	kg/m ³
ρ_0	RHO0	water density for reference water temperature and salt content		kg/m3
ρ_{A}	DNA, RHOA	Mass density of air	Mass of air per unit volume	kg/m ³
τ	ST, TAU	Tangential stress		Pa
λ	SC	Scale ratio	Ship dimension divided by corresponding model dimension	1
σ	SN, SIGS	Normal stress		Pa
ω	FC, OMF	Circular frequency	$2\pi f$	1/s
ω , V^0	V0, OMN	Rotational velocity	$2\pi n$	rad/s

ITTC	Computer	Nome	Definition or	SI-
Symbol	Symbol	Name	Explanation	Unit

2.2 Geometry and Hydrostatics2.2.1 Hull Geometry2.2.1.1 Basic Quantities

2.2.1.1 B	asic Quantities			
$A_{ m BL}$	ABL	Area of bulbous bow in longitudinal plane	The area of the ram projected on the middle line plane forward of the fore perpendicular	m^2
$A_{ m BT}$	ABT	Area of transverse cross-section of a bulbous bow (full area port and star-board)	The cross sectional area at the fore perpendicular. Where the water lines are rounded so as to terminate on the forward perpendicular $A_{\rm BT}$ is measured by continuing the area curve forward to the perpendicular, ignoring the final rounding.	m^2
A_{M}	AM	Area of midship section	Midway between fore and aft perpendiculars	m^2
A_{T}	ATR	Area of transom (full area port and starboard)	Cross-sectional area of transom stern below the load waterline	m^2
$A_{ m V}$	AV	Area exposed to wind	Area of portion of ship above waterline projected normally to the direction of relative wind	m^2
$A_{ m XV}$	AXV	the waterline including superstructures	Projected area of the ship above the waterline projected on a transversal plane	
$A_{ m W}$	AW	Area of water-plane		m^2
$A_{ m WA}$	AWA	Area of water-plane aft of midship		m^2
$A_{ m WF}$	AWF	Area of water-plane forward of midship		m^2
$A_{\rm X}$	AX	Area of maximum transverse section		m^2
В	В	Breadth, moulded, of ships hull		m
$B_{ m M}$	BM	Breadth, moulded of midship section at design water line		m
B_{T}	BTR	Breadth, moulded of transom at design water line		m
$B_{ m WL}$	BWL	Maximum moulded breadth at design water line		m
$B_{\rm X}$	BX	Breadth, moulded of maximum section area at design water line		m
d, T	T	Draught, moulded, of ship hull		m
$d_{ m KL}$	KDROP	Design drop of the keel line	T _{AD} - T _{FD} alias "keel drag" or "slope of keel"	m
D	DEP	Depth, moulded, of a ship hull		m
f	FREB	Freeboard	From the freeboard markings to the freeboard deck, according to official rules	m
$i_{ m E}$	ANEN	Angle of entrance, half	Angle of waterline at the bow with reference to centre plane, neglect- ing local shape at stem	rad
$i_{ m R}$	ANRU	Angle of run, half	Angle of waterline at the stern with reference to the centre-plane, neglecting local shape of stern frame	rad

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2.2.1 Hull Geometry

ITTC Computer Definition or SI-Name Symbol Symbol Explanation Unit Reference length of ship (gener-L L Length of ship ally length between the perpendicm ulars) From the forward perpendicular to the forward end of parallel middle $L_{\rm E}$ LEN Length of entrance m body, or maximum section LOA Length, overall L_{OA} m Length, overall submerged LOS $L_{\rm OS}$ m Length of constant transverse sec-LP $L_{\rm P}$ Length of parallel middle body m LPP Length between perpendiculars L_{PP} m From section of maximum area or after end of parallel middle body LRU $L_{\rm R}$ Length of run m to waterline termination or other designated point of the stern LWL Length of waterline m $L_{\rm WL}$ LFS used for structures $L_{\rm FS}$ Frame spacing m LSS Station spacing L_{SS} m S, AWS Area of wetted surface m^2 The intercept of the tangent to the ТТ Taylor tangent of the area curve sectional area curve at the bow on 1 the midship ordinate *T*, *d* Draught, moulded, of ship hull m TA, TAP T_A , d_A Draught at aft perpendicular m Design draught at aft perpendicu- $T_{\rm AD}$ TAD, TAPD m TF, TFP Draught at forward perpendicular $T_{\rm F}$, $d_{\rm F}$ m Design draught at forward perpen- $T_{\rm FD}$ TFD, TFPD m dicular Maximum draught of the hull T_H THUL Draught of the hull m without keel or skeg $(T_A + T_F) / 2$ for rigid bodies with $T_{\rm M}, d_{\rm M}$ TM, TMS Draught at midship m straight keel $(T_{AD} + T_{FD}) / 2$ for rigid bodies T_{MD} TMD, TMSD Design draught at midship m Vertical depth of trailing edge of $T_{\rm T}$ TTR Immersion of transom boat at keel below water surface m level ∇ . VDISPVOL m^3 Displacement volume $\Delta / (\rho g) = \nabla_{BH} + \nabla_{AP}$ DISPVBH Displacement volume of bare hull m^3 $\Delta_{\rm BH}/\left(\rho\;g\right)$ $V_{
m BH}$ Displacement volume of append m^3 $V_{\rm APP}$ DISPVAP $\Delta_{AP} / (\rho g)$ $g \rho \overline{\overline{V}}$ DISPF Displacement force (buoyancy) N 1 Displacement force (buoyancy) of N DISPFBH Δ_{BH} $g \rho V_{\rm BH}$ bare hull Displacement force (buoyancy) of N DISPFAP Δ_{APP} $g \rho V_{AP}$ appendages DISPM Displacement mass Δ_m kg $\lambda = L_{\rm S}/L_{\rm M} = B_{\rm S}/B_{\rm M}$ SC λ Linear scale of ship model $= T_{\rm S} / T_{\rm M}$ **Derived Quantities** 2.2.1.2 B^{C} CIRCB R.E. Froude's breadth coefficient $B / \nabla^{1/3}$ $\nabla / (L B T)$ $C_{\rm B}$ CB Block coefficient 1 CGM $\overline{GM}/\nabla^{1/3}$ $C_{\rm GM}$ Dimensionless GM coefficient

 $A_{\rm X}/(B\ T)$, where B and T are

 $\frac{\nabla/L^3}{A_{\rm BL}/(L\ T)}$

 $A_{\mathrm{BT}}/A_{\mathrm{X}}$

 $A_{\rm T}/A_{\rm X}$

 $L/\nabla^{1/3}$

 $S/\nabla^{2/3}$

 $T/\nabla^{1/3}$

measured at the position of maxi-

1

1

Version 2021 2.2.1 Hull Geometry

ITTC Symbol	Computer Symbol	Name	Definition or Explanation	SI- Unit
C_{GZ}	CGZ	Dimensionless \overline{GZ} coefficient	\overline{GZ} / $\overline{V}^{1/3}$	1
C_{KG}	CKG	Dimensionless \overline{KG} coefficient	\overline{KG} /T	1
$C_{I\!L}$	CWIL	Coefficient of inertia of water plane, longitudinal	$12 I_{\rm L}/(B L^3)$	1
C_{IT}	CWIT	Coefficient of inertia of water plane, transverse	$12 I_{\rm T} / (B^3 L)$	1
$C_{ m M}$	CMS	Midship section coefficient (mid- way between forward and aft per- pendiculars)	$A_{\rm M}/\left(B\ T\right)$	1
C_{P}	CPL	Longitudinal prismatic coefficient	$\nabla/(A_{\rm X} L)$ or $\nabla/(A_{\rm M} L)$	1
C_{PA}	CPA	Prismatic coefficient, after body	$V_{\rm A}/(A_XL/2)$ or $V_{\rm A}/(A_{\rm M}L/2)$	1
$C_{ ext{PE}}$	СРЕ	Prismatic coefficient, entrance	$\overline{V_{\rm E}}$ / $(A_{\rm X} L_{\rm E})$ or $\overline{V_{\rm E}}$ / $(A_{\rm M} L_{\rm E})$	1
$C_{ t PF}$	CPF	Prismatic coefficient fore body	$V_{\rm F}/(A_{\rm X}L/2)$ or $V_{\rm F}/(A_{\rm M}L/2)$	1
C_{PR}	CPR	Prismatic coefficient, run	$V_{\rm R}$ / $(A_{\rm X}L_{\rm R})$ or $V_{\rm R}$ / $(A_{\rm M}L_{\rm R})$	1
C_S	CS	Wetted surface coefficient	$S/(VL)^{1/2}$	1
$C_{ m VP}$	CVP	Prismatic coefficient vertical	$V/(A_WT)$	1
C_{WA}	CWA	Water plane area coefficient, aft	$A_{\rm WA}$ / (B L / 2)	1
$C_{ m WF}$	CWF	Water plane area coefficient, forward	A _{WF} /(B L / 2)	1
C_{WP}	CW	Water plane area coefficient	A_{W} /(L B)	1
		*	· · /	

Maximum transverse section coef-

Area coefficient for bulbous bow

Taylor sectional area coefficient

Sectional area coefficient for tran-

R.E. Froude's length coefficient, or

R.E. Froude's draught coefficient

length-displacement ratio
R.E. Froude's wetted surface area

Volumetric coefficient

for bulbous bow

som stern

coefficient

ficient

2.2.1.3 Symbols for Attributes and Subscripts

CX

CVOL

CABL

CABL

ATR

CIRCM

CIRCS

CIRCT

 $C_{\rm X}$

 C_{∇}

 $f_{\rm BL}$

 $f_{\rm BT}$

 $f_{\rm T}$

 M^{C}

 S^C

•		1
A	AB	After body
AP	AP	After perpendicular
APP	APP	Appendages
В	BH	Bare hull
	DW	Design waterline
E	EN	Entry
F	FB	Fore body
FP	FP	Fore perpendicular
FS	FS	Frame spacing
H	HE	Hull
	LR	Reference Line
LP	LP	Based on LPP
LW	LW	Based on LWL

2 Ships in General2.2 Geometry and Hydrostatics2.2.1 Hull Geometry

ITTC Symbol	Computer Symbol	Name	Definition or Explanation	SI- Unit
M	MS	Midships		
111	PB	Parallel body		
R	RU	Run		
SS	SS	Station spacing		
W	WP	Water plane		
S	WS	Wetted surface		

ITTC	Computer	Nome	Definition or	SI-
Symbol	Symbol	Name	Explanation	Unit

2.2.2 Propulsor Geometry 2.2.2.1 Screw Propellers

2.2.2.1 Scre	ew Propellers			
$A_{ m D}$	AD	Developed blade area	Developed blade area of a screw propeller outside the boss or hub	m^2
$A_{ m E}$	AE	Expanded blade area	Expanded blade area of a screw propeller outside the boss or hub	m^2
A_0	AO	Propeller Disc Area	$\pi D^2 / 4$	m^2
$A_{ m P}$	AP	Projected blade area	Projected blade area of a screw propeller outside the boss or hub	m^2
$a_{ m D}$	ADR	Developed blade area ratio	$A_{\mathrm{D}}/A_{\mathrm{0}}$	1
$a_{ m E}$	ADE	Expanded blade area ratio	$A_{\rm E}/A_0$	1
a_{P}	ADP	Projected blade area ratio	$A_{\rm P}/A_0$	1
С	LCH	Chord length		m
C _{0.7}	C07	Chord length	Chord length at r/R=0.7	m
$c_{ m LE}$	CHLE	Chord, leading part	The part of the Chord delimited by the Leading Edge and the intersec- tion between the Generator Line and the pitch helix at the consid- ered radius	m
$c_{ m M}$	СНМЕ	Mean chord length	The expanded or developed area of a propeller blade divided by the span from the hub to the tip	m
c_{S}	CS	Skew displacement	The displacement between middle of chord and the blade reference line. Positive when middle chord is at the trailing side regarding the blade reference line	m
c_{TE}	СНТЕ	Chord, trailing part	The part of the Chord delimited by the Trailing Edge and the intersec- tion between the Generator Line and the pitch helix at the consid- ered radius	m
$d_{ m h}$	DH	Boss or hub diameter	2 r _h	m
$d_{ m ha}$	DHA	Hub diameter, aft	Aft diameter of the hub, not considering any shoulder	m
$d_{ m hf}$	DHF	Hub diameter, fore	Fore diameter of the hub, not considering any shoulder	m
D	DP	Propeller diameter		m
f	FBP	Camber of a foil section		m
G_Z	GAP	Gap between the propeller blades	$2 \pi r \sin(\varphi) / z$	m
h_0	НО	Immersion	The depth of submergence of the propeller measured vertically from the propeller centre to the free surface	m
H_{TC}	HTC	Hull tip clearance	Distance between the propeller sweep circle and the hull	m
i_G , R_k (ISO)	RAKG	Rake	The displacement from the propeller plane to the generator line in the direction of the shaft axis. Aft displacement is positive rake.	m
$i_{ m S}$	RAKS	Rake, skew-induced	The axial displacement of a blade section which occurs when the propeller is skewed. Aft displace- ment is positive rake	m

2.2.2 Propulsor Geometry

ITTC Computer Definition or SI-Name Symbol Symbol Explanation Unit The axial displacement of the blade reference line from the pro-RAKT Rake, total peller plane m $i_{\rm G} + i_{\rm S} = c_{\rm S} \sin \varphi$ Positive direction is aft. The length of the hub, including LH Hub length $l_{
m h}$ any fore and aft shoulder Length of the hub taken from the LHA Hub length, aft propeller plane to the aft end of m l_{ha} the hub including aft shoulder Length of the hub taken from the propeller plane to the fore end of LHF Hub length, fore $l_{
m hf}$ m the hub including fore shoulder NPR Number of propellers $N_{\mathbf{P}}$ $\overline{P/D}$ PDR Pitch ratio 1 PITCH Propeller pitch in general m LR Blade section radius m Hub radius RH m R RDP Propeller radius m TM Blade section thickness m Thickness on axis of propeller Thickness of propeller blade as ex-TO m t_0 blade tended down to propeller axis XBDR Boss to diameter ratio $x_{\rm B}$ Distance of propeller centre for-ΧP Longitudinal propeller position m $x_{\rm P}$ ward of the after perpendicular Transverse distance of wing pro-ΥP Lateral propeller position m УP peller centre from middle line NPB Number of propeller blades Z, zHeight of propeller centre above ΖP Vertical propeller position m ZΡ Angle of inclination of the propel-Angle between propeller shaft and AAdeg α ler shaft horizontal Propeller axis angle measured to Angle between reference line and ε, ψ^{bP} PSIBP rad body fixed coordinates propeller shaft axis The angular displacement about the shaft axis of the reference point of any blade section relative $\theta_{
m s}$ TETS to the generator line measured in Skew angle rad the plane of rotation. It is positive when opposite to the direction of ahead rotation RAKA Angle of rake rad The difference between maximum rad TEMX Skew angle extent θ_{EXT} and minimum local skew angle PHIP Pitch angle of screw propeller $arctg(P/(2\pi R))$ Pitch angle of screw propeller PHIF $\varphi_{\rm F}$ measured to the face line Propeller axis angle measured to Angle between horizontal plane ψ^{aP} PSIAP rad space fixed coordinates and propeller shaft axis Blade thickness ratio t_0/D

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Version 2021

ITTC Symbol	Computer Symbol	Name	Definition or Explanation	SI- Unit
•	•		Explanation	Cilit
	icts	Durat autom and	1	12
A _{DEN}	ADEN ADEX	Duct entry area Duct exit area		m^2 m^2
A _{DEX}		Duct exit area	Clearance between propeller tip	III
$d_{ m D}$	CLEARD	Propeller tip clearance	and inner surface of duct	m
D	FD	Camber of duct profile		m
LD	LD	Duct length		m
DEN	LDEN	Duct entry part length	Axial distance between leading edge of duct and propeller plane	m
$L_{ m DEX}$	LDEX	Duct exit length	Axial distance between propeller plane and trailing edge of duct	m
^t D	TD	Thickness of duct profile		m
$\chi_{ m D}$	AD	Duct profile-shaft axis angle	Angle between nose-tail line of duct profile and propeller shaft	rad
β_{D}	BD	Diffuser angle of duct	Angle between inner duct tail line and propeller shaft	rad
.2.2.3 Wa	aterjets (see also	section 1.3.5)		•
A_n, A_6		Nozzle discharge area		m^2
$A_{\rm s}$		Cross sectional area at station s		m^2
\overline{D}		Impeller diameter (maximum)		m
$D_{\rm n}$		Nozzle discharge diameter		m
H_{ij}		Head between station <i>i</i> and <i>j</i>		m
$H_{ m JS}$		Jet System Head	$\frac{P_{ ext{JSE}}}{Q_{ ext{J}}}$	m
h_{1A}		maximum height of cross section area of stream tube at station 1A	al	m
$K_{\scriptscriptstyle H}$		Head coefficient:	$\frac{gH}{n^2D^5}$	1
.2.2.4 Po	ds			
$A_{ m PB}$	APB	Wetted Surface Area of Pod Main Body		m^2
$A_{ m PBF}$	APBF	Wetted Surface Area of Bottom Fin		m ²
4_{PS}	APS	Wetted Surface Area of Strut		m ²
Светс	CBFTC	Thickness Cord Ratio of Bottom Fin		1
Cstc	CSTC	Thickness Cord Ratio of Strut		1
D _{PB}	DPB	Maximum Diameter of Pod Body		m
$\mathcal{L}_{\mathrm{PB}}$	LPB	Length of Pod Main Body		m
PBF	LPBF	Length of Bottom Fin	Code length of bottom fin under pod main body	m
· -PS	LPS	Length of Upper Strut	Code length of strut between forward edge and aft edge	m
T_{PBS}	TPBS	Bottom Thickness of Strut	mara cage and art cage	m
.2.2.5 Op	perators and idea		1	1
op		solute (space) reference	(superscript)	
		dy axis reference	(superscript)	
		opeller shaft axis	(subscript)	
)	Du		(subscript)	

ITTC

Symbol

2.2.3 Appendage Geometry Version 2021

Name

Definition or	SI-
Explanation	Unit

Computer

Symbol

2.2.3 Appendage Geometry Related information may be found in Section 3.3.3 on Lifting Surfaces.

2.2.3.1 Basic Ouantities

$A_{\rm C}$ Bas	AC AC	Area under cut-up		m^2
$A_{\rm FB}$	AFB	Area of bow fins		m^2
$A_{\rm FR}$	AFR	Frontal area	Projected frontal area of an appendage	m^2
$A_{ m RF}$	AF	Projected flap area		m^2
$A_{\rm R}$	ARU	Lateral rudder area	Area of the rudder, including flap	m^2
$A_{ m RX}$	ARX	Lateral area of the fixed part of rudder		m^2
$A_{ m RP}$	ARP	Lateral area of rudder in the propeller race		m^2
$A_{ m RT}$	ART	Total lateral rudder area	$A_{\rm RX} + A_{ m Rmov}$	m^2
A_{FS}	AFS	Projected area of stern fins		m^2
$A_{ m SK}$	ASK	Projected skeg area		m^2
$S_{ m WBK}$	SWBK	Wetted surface area of bilge keels		m^2
c	СН	Chord length of foil section		m
c_{M}	CHME	Mean chord length	$A_{\rm RT}/S$	m
c_{R}	CHRT	Chord length at the root		m
c_{T}	CHTP	Chord length at the tip		m
f	FM	Camber of an aerofoil or a hydrofoil	Maximum separation of median and nose-tail line	m
$L_{ m F}$	LF	Length of flap or wedge	Measured in direction parallel to keel	m
t	TMX	Maximum thickness of an aerofoil or a hydrofoil	Measured normal to mean line	m
α_{FB}	ANFB	Bow fin angle		rad
α_{FS}	ANFS	Stern fin angle		rad
$\delta_{ ext{F}}$	DELFS	Flap angle (general)	Angle between the planing surface of a flap and the bottom before the leading edge	rad
$\delta_{ m W}$	DELWG	Wedge angle	Angle between the planing surface of a wedge and the bottom before the leading edge	rad
$\delta_{ ext{FR}}$	ANFR	Flanking rudder angle		rad
$\delta_{ ext{FRin}}$	ANFRIN	Assembly angle of flanking rudders	Initial angle set up during the assembly as zero angle of flanking rudders	rad
$\delta_{ m R}$	ANRU	Rudder angle		rad
$\delta_{ ext{RF}}$	ANRF	Rudder-flap angle		rad
$\lambda_{ m R}$	TARU	Rudder taper	$c_{\mathrm{T}}/c_{\mathrm{R}}$	1
λ_{FR}	TAFR	Flanking rudder taper		1
$\Lambda_{ m R}$	ASRU	Rudder aspect ratio	$b_{\mathrm{R}}^2/A_{\mathrm{RT}}$	1
I_{FR}	ASRF	Flanking rudder aspect ratio		

2.2.3.2 Identifiers for Appendages (Subscripts)

BK	Bilge keel
BS	Bossing
FB	Bow foil
FR	Flanking rudder
FS	Stern foil
KL	Keel
RU	Rudder
RF	Rudder flap

2 Ships in General2.2 Geometry and Hydrostatics2.2.3 Appendage Geometry

ITTC Symbol	Computer Symbol	Name	Definition or Explanation	SI- Unit
	SA	Stabilizer		
	SH	Shafting		
	SK	Skeg		
	ST	Strut		
	TH	Thruster		
	WG	Wedge		

2.2 Geometry and Hydrostatics2.2.4 Hydrostatics and Stability

ITTC	Computer	Nama	Definition or	SI-
Symbol	Symbol	Name	Explanation	Unit

2.2.4 Hydrostatics and Stability2.2.4.1 Points and Centres (Still under construction)

<u> 2.2.4.1 Poi</u>	nts and Centre	es (Still under construction)		
A		Assumed centre of gravity above keel used for cross curves of sta-		
		bility		
		Centre of flotation of added buoy-		
b		ant layer or centre of lost buoy-		
		ancy of the flooded volume		
В		Centre of buoyancy	Centroid of the underwater vol-	
			ume	
F		Centre of flotation of the water		
1		plane		
g		Centre of gravity of an added or		
		removed weight (mass)		
G		Centre of gravity of a vessel		
K		Keel reference		
M		Metacentre of a vessel	See subscripts for qualification	
			Longitudinal distance from refer-	
X_{CB} , L_{CB}	XCB	Longitudinal centre of buoyancy	ence point to the centre of buoy-	m
05, -05		(LCB)	ancy, B such as X _{MCF} from Mid-	
			ships	
	XCF	I 't 1' 1	Longitudinal distance from refer-	
$X_{ m CF}$, $L_{ m CF}$		Longitudinal centre of flotation	ence point to the centre of flota-	m
		(LCF)	tion, F such as X _{MCF} from Mid-	
			ships	
		I amaitudinal contra of hyayanay	Longitudinal distance from refer-	
$\mathcal{X}_{ ext{Cb}}$	XACB	Longitudinal centre of buoyancy	ence point to the centre of buoy-	m
		of added buoyant layer	ancy of the added buoyant layer, b	
			such as x_{MCb} from Midships Longitudinal distance from refer-	
		Longitudinal centre of flotation of	ence point to the centre of flota-	
χ_{Cf}	XACF	added buoyant layer	tion of the added buoyant layer, f	m
		added buoyant layer	such as x_{MCf} from Midships	
			Longitudinal distance from refer-	
			ence to the centre of gravity, g, of	
$x_{ m Cg}$	XACG	Longitudinal centre of gravity of	an added or removed weight	m
WCg		added weight (mass)	(mass) such as x_{MCg} from Mid-	
			ships	
			Longitudinal distance from a ref-	
	****	Longitudinal centre of gravity	erence point to the centre of grav-	
$X_{\rm CG}$, $L_{\rm CG}$	XCG	(LCG)	ity, G such as X _{MCG} from Mid-	m
			ships	
V	VCC	Lateral displacement of centre of	Lateral distance from a reference	
$Y_{\rm CG}$	YCG	gravity (YCG)	point to the centre of gravity, G	m
		Intersection of righting arm with		
Z	ZRA	line of action of the centre of		
		buoyancy		<u></u>
7	ZCB	Vertical centre of buoyancy	Vertical distance from reference	m
$Z_{\rm CB}$	LCD	vertical centre of buoyancy	point to the centre of buoyancy, B	m

2.2.4.2 Static Stability levers

\overline{AB} XAB Longitudinal centre of buoyancy from aft perpendicular	Distance of centre of buoyancy from aft perpendicular	m
--	---	---

ITTC Symbol	Computer Symbol	Name	Definition or Explanation	SI- Unit
\overline{AF}	XAF	Distance of centre of flotation from aft perpendicular		m
$\overline{AG}_{ m L}$	XAG	Longitudinal centre of gravity from aft perpendicular	Distance of centre of gravity from aft perpendicular	m
$\overline{AG}_{_{ m T}}$	YAG	Transverse distance from assumed centre of gravity A, to actual centre of gravity G		m
$\overline{AG}_{_{\mathrm{V}}}$	ZAG	Vertical distance from assumed centre of gravity A, to actual centre of gravity G		m
\overline{AZ}	YAZ	Righting arm based on horizontal distance from assumed centre of gravity A, to Z	Generally tabulated in cross curves of stability	m
\overline{BM}	ZBM	Transverse metacentre above centre of buoyancy	Distance from the centre of buoyancy B to the transverse metacentre M. $\overline{BM} = I_T / \nabla = \overline{KM} - \overline{KB}$	m
\overline{BM}_L	ZBML	Longitudinal metacentre above centre of buoyancy	\overline{KM}_L - \overline{KB}	
\overline{FB}	XFB	Longitudinal centre of buoyancy, L_{CB} , from forward perpendicular	Distance of centre of buoyancy from forward perpendicular	m
\overline{FF}	XFF	Longitudinal centre of floatation, L_{CF} , from forward perpendicular	Distance of centre of flotation from forward perpendicular	m
\overline{FG}	XFG	Longitudinal centre of gravity from forward perpendicular	Distance of centre of gravity from forward perpendicular	m
\overline{GG} H	GGH	Horizontal stability lever caused by a weight shift or weight addi- tion		m
$\overline{GG}_{ m L}$	GGL	Longitudinal stability lever caused by a weight shift or weight addition		m
$\overline{GG}_1, \overline{GG}_V$	GG1, GGV	Vertical stability lever caused by a weight shift or weight addition	$\overline{KG}_1 = \overline{KG}_0 + \overline{GG}_1$	m
\overline{GM}	GM	Transverse metacentric height	Distance of centre of gravity to the metacentre \overline{KM} \overline{KG}	m
$\overline{GM}_{ ext{Eff}}$	GMEFF	Effective transverse metacentric height	GM corrected for free surface and/or free communication effects	m
$\overline{GM}_{\mathrm{L}}$	GML	Longitudinal centre of metacentric height	Distance from the centre of gravity G to the longitudinal metacentre $\frac{M_L}{GM_L} = \overline{KM_L} - \overline{KG}$	m
\overline{GZ}	GZ	Righting arm or lever	$\overline{GZ} = \overline{AZ} - \overline{AG}_{V} \sin \varphi - \overline{AG}_{T} \cos \varphi$	m
$\overline{GZ}_{ ext{MAX}}$	GZMAX	Maximum righting arm or lever		m
KA	ZKA	Assumed centre of gravity above moulded base or keel	Distance from the assumed centre of gravity A to the moulded base or keel K	m

Ships in General Geometry and Hydrostatics Hydrostatics and Stability

ITTC Symbol	Computer Symbol	Name	Definition or Explanation	SI- Unit
Бушоот	Бушоог		Explanation	Omt
KB	ZKB	Centre of buoyancy above moulded base or keel	Distance from the centre of buoyancy B to the moulded base or keel K	m
\overline{KG}	ZKG	Centre of gravity above moulded base or keel	Distance from centre of gravity G to the moulded base or keel K	m
Kg	ZKAG	Vertical centre of gravity of added or removed weight above moulded base or keel	Distance from centre of gravity, g, to the moulded base or keel K	m
\overline{KM}	ZKM	Transverse metacentre above moulded base or keel	Distance from the transverse meta- centre M to the moulded base or keel K	m
\overline{KM}_L	ZKML	Longitudinal metacentre above moulded base or keel	Distance from the longitudinal metacentre M _L to the moulded base or keel K	m
1	XTA	Longitudinal trimming arm	$x_{\rm CG}$ - $x_{\rm CB}$	m
t	YHA	Equivalent transverse heeling arm	Heeling moment /∆	m
2.2.4.3 De	erived Quantities	5	1	
$C_{\rm GM}$	CGM	Dimensionless \overline{GM} coefficient	$\overline{GM}/\nabla^{1/3}$	1
C_{GZ}	CGZ	Dimensionless \overline{GZ} coefficient	\overline{GZ} / $\nabla^{1/3}$	1
C_{KG}	CKG	Dimensionless \overline{KG} coefficient	\overline{KG} /T	1
C_{MTL}	CMTL	Longitudinal trimming coefficient	Trimming moment divided by change in trim which approximately equals \overline{BM}_L/L	1
2.2.4.4 Int	tact and Damage	e (Flooded) Stability		
C_{MTL}	CMTL	Longitudinal trimming coefficient	trimming moment divided by change in trim which approximately equals $\overline{BM}_{\rm L}/L$	1
f	FREB	Freeboard	From the freeboard markings to the freeboard deck, according to official rules	m
$A_{\rm SI}, I_{\rm AS}$	ASI	Attained subdivision index	(to be clarified)	1
$M_{ m S}$	MS	Moment of ship stability in general	$\Delta \overline{GZ}$ Other moments such as those of capsizing, heeling, etc. will be represented by MS with additional subscripts as appropri-	Nm
			ate	
m	SHIPMA	Ship mass	ate W/g	kg
$m = M_{TC}$	SHIPMA MTC	Ship mass Moment to change trim by one centimetre		kg Nm/cm
		Moment to change trim by one		
$M_{T\mathrm{C}}$	MTC MTM RSI	Moment to change trim by one centimetre Moment to change trim by one meter Required subdivision index	W/g	Nm/cm
M _{TC} M _{TM} R _{SI} t _s , t _{KL}	MTC MTM RSI TRIM	Moment to change trim by one centimetre Moment to change trim by one meter Required subdivision index Static trim	W/g	Nm/cm Nm/m 1 m
M _{TC} M _{TM} R _{SI} t _s , t _{KL}	MTC MTM RSI TRIM SHIPWT	Moment to change trim by one centimetre Moment to change trim by one meter Required subdivision index Static trim Ship weight	W/g ΔC_{MTL} $T_{\text{A}} - T_{\text{F}} - d_{\text{KL}}$ $m g$	Nm/cm Nm/m 1 m N
M_{TC} M_{TM} R_{SI} t_s, t_{KL} W z_{SF}	MTC MTM RSI TRIM SHIPWT ZSF	Moment to change trim by one centimetre Moment to change trim by one meter Required subdivision index Static trim Ship weight Static sinkage at FP	W/g $\Delta C_{\rm MTL}$ $T_{\rm A}$ - $T_{\rm F}$ - $d_{\rm KL}$ $m g$ Caused by loading	Nm/cm Nm/m 1 m N
M_{TC} M_{TM} R_{SI} t_s , t_{KL} W z_{SF}	MTC MTM RSI TRIM SHIPWT ZSF ZSA	Moment to change trim by one centimetre Moment to change trim by one meter Required subdivision index Static trim Ship weight Static sinkage at FP Static sinkage at AP	W/g $\Delta C_{\rm MTL}$ $T_{\rm A}$ - $T_{\rm F}$ - $d_{\rm KL}$ $m g$ Caused by loading Caused by loading	Nm/cm Nm/m 1 m N m m
M_{TC} M_{TM} R_{SI} t_s, t_{KL} W z_{SF}	MTC MTM RSI TRIM SHIPWT ZSF	Moment to change trim by one centimetre Moment to change trim by one meter Required subdivision index Static trim Ship weight Static sinkage at FP	W/g $\Delta C_{\rm MTL}$ $T_{\rm A}$ - $T_{\rm F}$ - $d_{\rm KL}$ $m g$ Caused by loading	Nm/cm Nm/m 1 m N

2.2.4 Hydrostatics and Stability

ITTC	Computer	Name	Definition or	SI-
Symbol	Symbol	Name	Explanation	Unit
Δ	DISPF	Displacement (buoyant) force	$g \rho \nabla$	N
Δ_m	DISPM	Displacement mass	$\rho \nabla$	kg
\overline{V}	DISPVOL	Displacement volume	Δ / (ρg)	m^3
$V_{ m fw}$	DISVOLFW	Displacement volume of flooded water	$\Delta f_w / (\rho g)$	m ³
$\theta_{ m S}$	TRIMS	Static trim angle	$\tan^{-1}((z_{SF} - z_{SA})/L)$	rad
μ	PMVO	Volumetric permeability	The ratio of the volume of flooding water in a compartment to the total volume of the compartment	1
ϕ	HEELANG	Heel angle		rad
ϕ_{F}	HEELANGF	Heel angle at flooding		rad
$\phi_{ m VS}$	HEELANGV	Heel angle for vanishing stability		rad

2.2.4.5 Symbols for Attributes and Subscripts (under construction)

a	apparent
A, att	attained
d, dyn	dynamic
e, EFF	effective
f	false
KL	keel line
L	longitudinal
MAX	maximum

MTL longitudinal trimming moment R, req required (to be clarified)

s Static

S, sqt Sinkage, squat TC Trim in cm TM Trim in m transverse V vertical 0 Initial

 ϕ at heel angle ϕ at trim angle θ

2 2	4	TT II D 1 4	
2.3		Hull Resistance	

ITTC	Computer	Name	Definition or	SI-
Symbol	Symbol	Name	Explanation	Unit

2.3 Resistance and Propulsion

2.3.1 Hull Resistance

(see also Section 1.4.1 on Waves) 2.3.1.1 Basic Quantities

Basic Quantities			
BLCK	Blockage parameter	Maximum transverse area of model ship divided by tank cross section area	1
RA	Model-ship correlation allowance	Incremental resistance to be added to the smooth ship resistance to complete the model-ship predic- tion	N
RAA	Air or wind resistance		N
RAP	Appendage resistance		N
RAR	Roughness resistance		N
RC	Resistance corrected for difference in temperature between resistance and self-propulsion tests	where C_{FMC} is the frictional coefficient at the temperature of the self-	N
RF	Frictional resistance of a body	Due to fluid friction on the surface	N
RF0	Frictional resistance of a flat plate		N
RP	Pressure resistance	Due to the normal stresses over the surface of a body	N
RPV	Viscous pressure resistance	Due to normal stress related to vis-	N
RR	Residuary resistance	-	N
RRBH	Residuary resistance of the bare hull		N
RS	Spray resistance	Due to generation of spray	N
RT	Total resistance	Total towed resistance	N
RTBH			N
RV		$R_{ m F}+R_{P m V}$	N
RW			N
RWB	Wave breaking resistance	Associated with the breakdown of	N
RWP	Wave pattern resistance		N
S		$S_{\rm BH} + S_{\rm APP}$	m^2
S0	Wetted surface area, at rest	$S_{ m BH0} + S_{ m APP0}$	m^2
SAP	Appendage wetted surface area, underway		m ²
SAP0	Appendage wetted surface area, at rest		m^2
SBH	Bare Hull wetted surface area, un- derway		m^2
SBH0	Bare Hull wetted surface area, at rest		m^2
DELCF	Roughness allowance		1
V	Speed of the model or the ship		m/s
VKN	Speed in knots		
VWR	Wind velocity, relative		m/s
ZVF	Running sinkage at FP		m
ZVA	Running sinkage at AP		m
	RA RAA RAP RAR RAP RAR RC RF RF0 RP RPV RR RRBH RS RT RTBH RV RW RWB RWP S S0 SAP SAP0 SBH SBH0 DELCF V VKN VWR ZVF	BLCK Blockage parameter RA Model-ship correlation allowance RAA Air or wind resistance RAP Appendage resistance RAP Roughness resistance Resistance corrected for difference in temperature between resistance and self-propulsion tests RF Frictional resistance of a body RF0 Frictional resistance of a flat plate RP Pressure resistance RPV Viscous pressure resistance RR Residuary resistance RRBH Residuary resistance RT Total resistance RT Total resistance RTBH Total resistance RWW Wave making resistance RWB Wave breaking resistance RWP Wave pattern resistance S Wetted surface area, underway SO Wetted surface area, at rest Appendage wetted surface area, underway SAP Appendage wetted surface area, at rest SAP Appendage wetted surface area, at rest SBH Bare Hull wetted surface area, underway SBHO Bare Hull wetted surface area, at rest DELCF Roughness allowance V Speed of the model or the ship VKN Speed in knots VWR Wind velocity, relative ZVF Running sinkage at FP	BLCK Blockage parameter Maximum transverse area of model ship divided by tank cross section area Incremental resistance to be added to the smooth ship resistance to complete the model-ship prediction RAA Air or wind resistance RAP Appendage resistance RC Resistance corrected for difference in temperature between resistance and self-propulsion tests RF Frictional resistance of a body RFO Frictional resistance of a flat plate RP Pressure resistance RR RRBH Residuary resistance RR RS Spray resistance RTBH Total resistance of the bare hull RV Total viscous resistance RTBH Total resistance of bare hull RV Wave making resistance RWB Wave breaking resistance S Wetted surface area, at rest SAPO Appendage wetted surface area, underway SAPO Appendage wetted surface area, underway SAPO Bare Hull wetted surface area, underway SBHO Bare Hull wetted surface area, underway Vixon Speed in knots VWR Wind velocity, relative ZVF Running sinkage at FP

ITTC	Computer		Definition or	SI-
Symbol	Symbol	Name	Explanation	Unit
25111001	z jilio o i		2.1	01111
$z_{V m M}$	ZVM	Mean running sinkage	$(z_{VF} + z_{VA})/2$	m
n	EW	Wave Elevation	see 3.4.1	m
θ_V , θ_D	TRIMV	Running (dynamic) trim angle	$\tan^{-1}((z_{VF} - z_{VA})/L)$	1
$ au_{ m W}$	LSF, TAUW	Local skin friction	see 3.3.4	N/m^2
	erived Quantities	I.	1	1
		Incremental resistance coefficient		
C_{A}	CA	for model ship correlation		1
		Tor moder ship correlation	$R_{AA}/(Sq)$	
$C_{ m AA}$	CAA	Air or wind resistance coefficient	$= C_{DA} \frac{\rho_A}{\rho_S} \frac{A_V}{S_S} = -C_X \frac{\rho_A}{\rho_S} \frac{A_V}{S_S}$	1
C_{APP}	CAPP	Appendage resistance coefficient	$R_{APP}/(S q)$	1
C_D	CD	Drag coefficient	D/(Sq)	1
C_{DA}	CDA	Air or wind resistance coefficient, from wind tunnel tests		1
C_{F}	CF	Frictional resistance coefficient of a body		1
$C_{ m F0}$	CF0	Frictional resistance coefficient of a corresponding plate	R_{F0} / (S q)	1
C_p	CP	Local pressure coefficient		1
C_{PR}	CPR	Pressure resistance coefficient, including wave effect	$R_P / (S q)$	1
$C_{P m V}$	CPV	Viscous pressure resistance coef- ficient	$R_{PV} / (S q)$	1
C_{R}	CR	Residuary resistance coefficient	$R_{\rm R} / (S q)$	1
C_{S}	CSR	Spray resistance coefficient	$R_{\rm S} / (Sq)$	1
C_{T}	CT	Total resistance coefficient	$R_{\mathrm{T}} / (S q)$	1
C_{TL}	CTLT	Telfer's resistance coefficient	$gRL/(\Delta V^2)$	1
C_{TQ}	CTQ	Qualified resistance coefficient	$C_{ m TV} / (\eta_{ m H} \eta_{ m R})$	1
$C_{\mathrm{T} \overline{V}}$	CTVOL	Resistance displacement	$R_{\mathrm{T}} / (\overline{V}^{2/3} q)$	1
$C_{ m V}$	CV	Total viscous resistance coeffi-	$R_{\rm V} / (S q)$	1
C_{W}	CW	Wave making resistance coeffi- cient	$R_{\mathrm{W}} / (S q)$	1
$C_{ m WP}$	CWP	Wave pattern resistance coeffi- cient, by wave analysis		1
C_{X}	CXA	Air or wind resistance coefficient, usually from wind tunnel tests	$-R_{\mathrm{AA}}/\left(A_{\mathrm{V}}q_{\mathrm{R}}\right)$	1
C ^c	CIRCC	R.E. Froude's resistance coefficient	$1000 R_{\rm T} / (\Delta (K^{\rm C})^2)$	1
F^{C}	CIRCF	R.E. Froude's frictional resistance coefficient	$1000 R_{\rm F} / (\Delta (K^{\rm C})^2)$	1
f	FC	Friction coefficient	Ratio of tangential force to normal force between two sliding bodies	1
k	K	Three dimensional form factor on flat plate friction	$(C_{\rm V}$ - $C_{\rm F0})$ / $C_{\rm F0}$	1
$k(\theta)$	WDC	Wind direction coefficient	C_{AA}/C_{AA0}	1
K^C	CIRCK	R.E. Froude's speed displacement coefficient	$(4 \pi)^{1/2} Fr_V \text{ or } (4\pi/g)^{1/2} V_K / V^{1/6}$	
K_R	KR	Resistance coefficient corresponding to K_Q , K_T	$R/(\rho D^4 n^2)$	1
q	PD, EK	Dynamic pressure, density of kinetic flow energy,	$\rho V^2 / 2$ see 3.3.2	Pa

Resistance and Propulsion 2.3

2.3.1 Hull Resistance

ITTC Symbol	Computer Symbol	Name	Definition or Explanation	SI- Unit
$q_{ m R}$	PDWR, EKWR	Dynamic pressure based on apparent wind	$\rho V_{WR}^2 / 2$ see 3.4.2	Pa
S^{C}	CIRCS	R. E. Froude's wetted surface coefficient	$S/V^{2/3}$	1
ε	EPSG	Resistance-displacement ratio in general	R/Δ	1
$arepsilon_{ m R}$	EPSR	Residuary resistance-displace- ment ratio	$R_{ m R}$ / Δ	1

$\frac{\varepsilon_{\rm R}}{2.3.1.3}$ Symbols for Attributes and Subscripts

FWFresh water MF Faired model data Raw model data MR Open water Faired full scale data OW

SF Raw full scale data SR

SWSalt water

ITTC	Computer	Name	Definition or	SI-
Symbol	Symbol	Name	Explanation	Unit

2.3.2 Ship Performance2.3.2.1 Basic Quantities

$A_{ m XV}$	AXV	Transverse projected area above the waterline including superstruc-	Projected area of the ship above the	
¹XV	7171 V	tures	plane	
⁷ D	SFC	Friction deduction force in self propulsion test	Towing force applied to a model to correct the model resistance for different <i>Re</i> between model and full scale.	N
r' _P	FP	Force pulling or towing a ship		N
F _{P0}	FPO	Pull during bollard test		N
ζ_S	KHS	Roughness height of Hull surface		m
η	N	Frequency, commonly rate of revolution		Hz
P _B	PB	Brake power	Power delivered by prime mover	W
P_{BW}	PBW	Brake power in representative sea condition		W
$P_{ m D}$, $P_{ m P}$	PD, PP	Delivered power, propeller power	$Q \omega$	W
$P_{\mathrm{D}T}$	PDT	Delivered Power, corrected using correlation factor	$P_{\rm DT} = C_P \cdot P_{\rm DS}$	W
$P_{\rm E}$, P_R	PE, PR	Effective power, resistance power	RV	W
P_{I}	PI	Indicated power	Determined from pressure measured by indicator	W
$P_{\rm S}$	PS	Shaft power	Power measured on the shaft	W
$P_{\rm S}$ P_{T}	PTH	Thrust power	$T V_{\rm A}$	W
Q	Q	Torque	$P_{ m D}/\omega$	Nm
R_0	R0	Full scale resistance without over-load		N
R_{Tw}	RTW	Total resistance in wind and waves		N
† _V	TV	Running trim		m
\overline{V}	V	Ship speed		m/s
$V_{ m A}$	VA	Propeller advance speed	Equivalent propeller open water speed based on thrust or torque identity	m/s
$V_{ m ref}$	VREF	Design ship speed when the ship is in operation in a calm sea condi- tion (no wind and waves)		m/s
$V_{ m w}$	VW	Design ship speed when the ship is in operation under the representa- tive sea condition		m/s
ZV	ZV	Running sinkage of model or ship		m
ω	V0,OMN	Rotational shaft velocity	$2 \pi n$	1/s

а	RAUG	Resistance augment fraction	$(T - R_{\rm T}) / R_{\rm T}$	1
$B_{ m f}$	BF	Bluntness coefficient	7.5-04-01-01.1	1
C_{ADM}	CADM	Admiralty coefficient	$\Delta^{2/3} V^3 / P_{\rm S}$	1
$C_{\mathrm{D} \mathit{V}}$	CDVOL	Power-displacement coefficient	$P_D / (\rho V^3 \nabla^{2/3} / 2)$	1
C_N	CN	Trial correction for propeller rate of revolution at speed identity	$n_{\mathrm{T}} / n_{\mathrm{S}}$	1
C_{NP}	CNP	Trial correction for propeller rate of revolution at power identity	$P_{ m DT}/P_{ m DS}$	1
C_P	CDP	Trial correction for delivered power		1

2.3.2 Ship Performance

Version 2021

EFGP

ITTC Computer Definition or SI-Name Symbol Symbol Unit Explanation speed in wind and waves Weather factor, a non-dimensional coefficient indicating the decrease speed in calm water FWE f_{w} of speed in representative sea con-Ship model correlation factor for K_1 C1 $\eta_{\mathrm{DS}}/\eta_{\mathrm{DM}}$ propulsive efficiency Ship model correlation factor for K_2 C2 $n_{\rm S}/n_{\rm M}$ propeller rate revolution Scale effect correction factor for model appendage drag applied at KAP K_{APP} Appendage correction factor the towing force in a self-propulsion test Change of draught, fore and aft, SINKV Sinkage, dynamic SVdivided by length Change of the trim due to dynamic TRIMV Trim, dynamic t_V condition, divided by length THDF Thrust deduction fraction $(T - R_T) / T$ $(V - V_{\rm A}) / V$ WFT Taylor wake fraction in general w WFF $(V - V_{\rm A}) / V_{\rm A}$ Froude wake fraction $w_{\rm F}$ Propeller speed V_A determined w_Q WFTQ Torque wake fraction from torque identity Effect of the rudder(s) on the wake $w_{\rm R}$ fraction Propeller speed, V_A , determined WFTT w_T Thrust wake fraction from thrust identity ∆R_{waves} DRWA Added wave resistance N DRWI Added wind resistance ΔR_{wind} Ship-model correlation factor for DELW 1 Δw $w_{T,M}$ - $w_{T,S}$ wake fraction Ship-model correlation factor with **DELWC** $\Delta w_{\rm C}$ respect to $w_{T,S}$ method formula of ITTC 1978 method XLO Load fraction in power prediction $\eta_{\rm D} P_{\rm D}/P_{\rm E}$ - 1 Ship appendage resistance divided APSF Appendage scale effect factor by model appendage resistance Load variation coefficient of the ξ_n shaft revolution speed Load variation coefficient of the ξ_P delivered power Load variation coefficient of the ξ_V ship speed Efficiencies etc. 2.3.2.3 ETAAP Appendage efficiency $P_{\text{Ew0APP}} / P_{\text{EwAPP}}$, $R_{\text{TBH}} / R_{\text{T}}$ $\eta_{
m APP}$ ETAB, $P_{\rm T}/P_{\rm D} = T V_{\rm A}/(Q \omega)$ Propeller efficiency behind ship 1 η_{B} EFTP Quasi-propulsive efficiency coef-ETAD, $P_{\rm E}/P_{\rm D} = P_{\rm R}/P_{\rm P}$ 1 $\eta_{\rm D}$ **EFRP** Propulsive efficiency in ideal con-**ETADID** $\eta_{
m Did}$ dition, from model test ETAG, Gearing efficiency η_{G}

ITTC	Computer	Name	Definition or	SI-
Symbol	Symbol	rame	Explanation	Unit
$\eta_{ m H}$	ETAH, EFRT	Hull efficiency	$P_{\rm E} / P_{\rm T} = P_{\rm R} / P_{\rm T}$ = $(1 - t) / (1 - w)$	1
$\eta_{ m M}$	ETAM	Mechanical efficiency of transmission between engine and propeller	$P_{ m D}/P_{ m B}$	1
$\eta_{\rm O}$	ETAO, EFTPO	Propeller efficiency in open water	$P_{\rm T}/P_{\rm D} = T V_{\rm A}/(Q \omega)$ all quantities measured in open water tests	1
$\eta_{ m P}$	ETAP	Propulsive efficiency coefficient	$P_{ m E}/P_{ m B}$	1
$\eta_{ m R}$	ETAR, EFRO	Relative rotative efficiency	$\eta_{ m B}/\eta_{ m O}$	1
$\eta_{ m S}$	ETAS, EFPS	Shafting efficiency	$P_{\rm D}/P_{\rm S} = P_{\rm P}/P_{\rm S}$	1

ITTC	Computer	Name	Definition or	SI-
Symbol	Symbol	Name	Explanation	Unit

2.3.3 Propulsor Performance2.3.3.1 Basic Quantities

	asic Quantities	n		1 2
$A_{\rm O}$	AO	Propeller disc area	$\pi D^2 / 4$	m ²
D	DP	Propeller diameter		m
n	FR	Propeller frequency of revolution		Hz
$n_{ m T}$		Propeller rate of revolution, corrected using correlation factor	$n_{\rm T} = C_N \cdot n_{\rm S}$	1
$k_{ m P}$	KS	Roughness height of propeller blade surface		m
$q_{ m A}$	QA	Dynamic pressure based on advance speed	$\rho V_{\rm A}^2 / 2$	Pa
q_{S}	QS	Dynamic pressure based on section advance speed	$\rho V_{\rm S}^2 / 2$	Pa
Q_{S}	QSP	Spindle torque	About spindle axis of controllable pitch propeller $Q_S=Q_{SC}+Q_{SH}$ positive if it increases pitch	Nm
$Q_{ m SC}$	QSPC	Centrifugal spindle torque		Nm
Q_{SH}	QSPH	Hydrodynamic spindle torque		Nm
$R_{ m U}$	RU	Pod unit resistance	Resistance of a podded drive unit	N
T	TH	Propeller thrust	•	N
$T_{ m U}$	TU	Pod unit thrust	Pod unit resistance subtracted from the propeller thrust	N
$T_{ m D}$	THDU	Duct thrust of a ducted propeller unit		N
$T_{ m P}$	THDP	Propeller thrust of a ducted propeller unit		N
T_{T}	THDT	Total thrust of a ducted propeller unit		N
T_{xP}	TXP	Propeller Thrust along shaft axis		N
T_{yP}	TYP	Propeller normal force in y direction in propeller axis		N
T_{zP}	TZP	Propeller normal force in z direction in propeller axis		N
$V_{\rm A}$	VA	Advance speed of propeller		m/s
V_{P}	VP	Mean axial velocity at propeller plane of ducted propeller		m/s
V_{S}	VS	Section advance speed at 0.7 R	$(V_{\rm A}^2 + (0.7 R \omega)^2)^{1/2}$	m/s
Y_U	YU	Pod unit side force		N
χ		Resistance fraction for one propeller	The portion of the resistance (load fraction, γ_i) that the i th propeller is responsible for	
ρ_{P}	DNP	Propeller mass density		kg/m ³
$ au_1$		Thrust deduction sensitivity for one propeller	$\tau_i = 1 + \left(\frac{\Delta F}{\Delta T}\right)_i$	1
ω	V0P	Propeller rotational velocity	$2\pi n$	1/s

2.3.3.2 Derived Quantities

4	2.3.3.2 DC11VC	a Quantities			
				$n P_{\rm D}^{V_2} / V_{\rm A}^{2.5}$	
	$B_{\rm P}$	BP	Taylor's propeller coefficient	with n in revs/min,	1
	D _P	DI	based on delivered horsepower	$P_{\rm D}$ in horsepower, and	1
				$V_{\rm A}$ in kn (obsolete)	

ITTC	Computer	Name	Definition or	SI-
Symbol	Symbol	Name	Explanation	Unit
			$n P_{\rm T}^{1/2} / V_{\rm A}^{2.5}$	
$B_{ m U}$	BU	Taylor's propeller coefficient	with n in revs/min,	1
B_0	Be	based on thrust horsepower	$P_{\rm T}$ in horsepower, and	1
			V _A in kn (obsolete)	
C_P	CPD	Power loading coefficient	$P_{\rm D}$ / $(A_{\rm P} q_{\rm A} V_{\rm A})$	1
C_{Q^*}	CQS	Torque index	$Q/(A_{\rm P} q_{\rm S} D)$	1
C_{Th}	СТН	Thrust loading coefficient, energy loading coefficient	$T/(A_{\rm P} q_{\rm A}) = (T_{\rm P}/A_{\rm P})/q_{\rm A}$	1
C_{T^*} J	CTHS	Thrust index	$T/(A_{\rm P} q_{\rm S})$	1
J	JEI	Propeller advance ratio	$V_{\rm A}/(D n)$	1
$J_{ m A}$, $J_{ m H}$	JA, JH	Apparent or hull advance ratio	$V/(D n) = V_{\rm H}/(D n)$	1
$J_{ m P}$	JP	Propeller advance ratio for ducted propeller	$V_{\rm P}$ / (D n)	
J_T , $J_{\mathrm PT}$	JT, JPT	Advance ratio of propeller deter-		1
7,011		mined from thrust identity		
J_{Q} , $J_{\mathrm{P}Q}$	JQ, JPQ	Advance ratio of propeller deter-		1
		mined from torque identity	D /(3 D5) 2 V	1
$K_P = K_Q$	KP	Delivered power coefficient	$P_{\rm D} / (\rho n^3 D^5) = 2 \pi K_Q$	1
K_Q	KQ	Torque coefficient	$Q/(\rho n^2 D^5)$	1
$K_{ m SC}$	KSC	Centrifugal spindle torque coefficient	$Q_{\rm SC} / (\rho n^2 D^5)$	1
$K_{ m SH}$	KSH	Hydrodynamic spindle torque co- efficient	$Q_{\rm SH}$ / ($\rho n^2 D^5$)	1
K_T	KT	Thrust coefficient	$T/(\rho n^2 D^4)$	1
$K_{T\mathrm{D}}$	KTD	Duct thrust coefficient for a ducted propeller unit	$T_{\rm D}$ / (ρ n^2 D^4)	1
K_{TP}	KTP	Propeller thrust coefficient for a ducted propeller unit	$T_{\rm P}$ / (ρ n^2 D^4)	1
K_{TQ}	KTQ	Thrust coefficient achieved by torque identity		1
$K_{T\Gamma}$	KTT	Total thrust coefficient for a ducted propeller unit	$K_{TP} + K_{TD}$	1
		Torque coefficient of propeller		
K_{Q0}	KQ0	converted from behind to open water condition	$K_{\mathcal{Q}}\eta_{\mathrm{R}}$	1
		Torque coefficient of propeller de-		
K_{QT}	KQT	termined from thrust coefficient identity		1
P_{J}	PJ	Propeller jet power	$\eta_{\mathrm{TJ}} T V_{\mathrm{A}}$	
S_{A}	SRA	Apparent slip ratio	1 - V/(nP)	1
$S_{ m R}$	SRR	Real slip ratio	$1 - V_A / (nP)$	1
δ	ADCT	Taylor's advance coefficient	$n D / V_A$ with n in revs/min, D in feet, V_A	1
			in kn	
$\eta_{ m JP}$	EFJP	Propeller pump or hydraulic effi- ciency	$P_{\rm J}/P_{\rm D} = P_{\rm J}/P_{\rm P}$	1
	7ET0	Propeller pump efficiency at zero		
$\eta_{ m JP0}$	ZET0, EFJP0	advance speed,	$T/(\rho \pi/2)^{1/3}/(P_{\rm D}D)^{2/3}$	1
		alias static thrust coefficient		
$\eta_{ m I}$	EFID	Ideal propeller efficiency	Efficiency in non-viscous fluid	1
$\eta_{ m TJ}$	EFTJ	Propeller jet efficiency	$2/(1+(1+C_{Th})^{1/2})$	1
η_0 , $\eta_{ ext{TP0}}$	ETA0, EFTP0	Propeller efficiency in open water	$P_{\rm T}/P_{\rm D} = T V_{\rm A}/(Q \omega)$ all quantities measured in open water tests	1
λ	ADR	Advance ratio of a propeller	$V_{\rm A}/(nD)/\pi = J/\pi$	1

2.3.3 Propulsor Performance

Version 2021

ITTC SI-Computer Definition or Name Symbol Symbol Explanation Unit Ratio between propeller thrust and TMR $T_{\rm P}/T_{\rm T}$ 1 total thrust of ducted propeller Induced Velocities etc. 2.3.3.3 Axial velocity induced by propel-UA $U_{\rm A}$ m/s Axial velocity induced by duct of U_{AD} UADU m/sducted propeller Radial velocity induced by propel- $U_{\rm RP}$ URP m/s ler of ducted propeller Radial velocity induced by duct of $U_{\rm RD}$ URDU m/s ducted propeller Axial velocity induced by propel- $U_{\rm AP}$ UAP m/s ler of ducted propeller Radial velocity induced by propel- $U_{\rm R}$ UR m/s Tangential velocity induced by U_{TD} UTDU m/s duct of ducted propeller Tangential velocity induced by U_{TP} UTP m/spropeller of ducted propeller Tangential velocity induced by U_{T} UT m/s propeller Advance angle of a propeller blade BETB $arctg(V_A/r\omega)$ rad section Hydrodynamic flow angle of a Flow angle taking into account in-BETI rad propeller blade section duced velocity BETS Effective advance angle $arctg (V_A/(0.7 R \omega))$ rad

ITTC

Symbol

2.3 Resistance and Propulsion2.3.4 Unsteady Propeller Forces Version 2021

Name

Definition or	SI-
Explanation	Unit

2.3.4 Unsteady Propeller Forces2.3.4.1 Basic Quantities

Computer

Symbol

	asic Quantities			
C_{uv}	SI(U,V)	Generalized stiffness		
D_{uv}	DA(U,V)	Generalized damping		
F_u	FG(I)	Generalized vibratory force	u = 1,, 6 u = 1, 2, 3: force u = 4, 5, 6: moment	N N Nm
$\overline{F_i}$	F(I)	Vibratory force	i = 1, 2, 3	N
K_{Fu}	KF(U)	Generalized vibratory force coeffi- cients		1
K_{Fi}	KF(I)	Vibratory force coefficients	$F_i/(\rho n^2 D^4)$	1
K_{Mi}	KM(I)	Vibratory moment coefficients	$M_i/(\rho n^2 D^5)$	1
K_p	KPR	Pressure coefficient	$p/(\rho n^2 D^2)$	1
M_i	M(I)	Vibratory moment	i = 1, 2, 3	Nm
M_{uv}	MA(U,V)	Generalized mass		
p	PR	Pressure		Pa
R_u	R(U)	Generalized vibratory bearing reaction	u = 1,, 6 u = 1, 2, 3: force u = 4, 5, 6: moment	N N Nm
$\overline{V_i}$	V(I)	Velocity field of the wake	i = 1, 2, 3	m/s
x y z	X Y Z	Cartesian coordinates	Origin O coinciding with the centre of the propeller. The longitudinal <i>x</i> -axis coincides with the shaft axis, positive forward; the transverse <i>y</i> -axis, positive to port; the third, <i>z</i> -axis, positive upward	m m m
X a r	X ATT R	Cylindrical coordinates	Cylindrical system with origin O and longitudinal <i>x</i> -axis as defined before; angular a-(attitude)-coordinate, zero at 12 o'clock position, positive clockwise looking forward; <i>r</i> distance measured from the <i>x</i> -axis	m 1 m
$\delta_{_{u}}$	DP(U)	Generalized vibratory displacement	u = 1,, 6 u = 1, 2, 3: linear u = 4, 5, 6: angular	m m rad
$\dot{\delta}_{\scriptscriptstyle u}$	DPVL(U)	Generalized vibratory velocity	u = 1,, 6 u = 1, 2, 3: linear u = 4, 5, 6: angular	m/s m/s rad/s
$\ddot{\mathcal{S}}_{u}$	DPAC(U)	Generalized vibratory acceleration	u = 1,, 6	m/s^2 m/s^2 rad/s^2

ITTC	Computer	Name	Definition or	SI-
Symbol	Symbol	Name	Explanation	Unit

C_p	СР	Local pressure coefficient	$(p-p_0)/(\rho V^2/2)$	1
C_{Tn}		Thrust loading coefficient:viscous pressure	$\frac{T_{\text{net}}}{\frac{1}{2}\rho U_0^2 A_{\text{n}}}$	1
es es		Energy velocity coefficient at station s		1
C _{ms}		Momentum velocity coefficient at station <i>s</i>		1
Dp		Pressure differential of flow rate transducer		Pa
\mathcal{E}_{j}	EJ	Energy flux at station j	$E_j = (\rho/2) \int V_{Ej}^2 dQ_j$ Q_J	W
$E_{ m s}$		Total energy flux at station s (kinetic + potential + pressure)	$ \iint_{A_s} \rho \left(\frac{1}{2} \mathbf{u}^2 + \frac{p}{\rho} - g_j x_j \right) u_i n_i dA $ $ \iint_{A_s} \rho \left(\frac{1}{2} u_{\xi}^2 + \frac{p}{\rho} - g_j x_j \right) u_i n_i dA $	W
$E_{{ m s} arxi}$		Total axial (in ξ direction) energy flux at station s	$\iiint_{A_s} \rho \left(\frac{1}{2} u_{\xi}^2 + \frac{p}{\rho} - g_j x_j \right) u_i n_i dA$	W
$F_{\scriptscriptstyle D}$		Skin friction correction in a self propulsion test carried out at the ship self-propulsion point		N
H_1	HT1	Local total head at station 1		m
H_{35}	Н35	Mean increase of total head across pump and stator or several pump stages		m
VR	IVR	Intake velocity ratio	VI/V	1
VR	JVR	Jet velocity ratio	VJ/V	1
K_Q		Impeller torque coefficient:	$\frac{Q}{\rho n^2 D^5}$ $\frac{Q_{\rm J}}{nD^3}$	
$K_{{\cal Q}^{ m J}}$		Flow rate coefficient:	$\frac{Q_{\rm J}}{nD^3}$	1
\overline{M} is		Momentum flux at station s in i direction	$\iint\limits_{A_s} \rho u_i (u_j n_j) dA$	N
NVR		Nozzle velocity ratio:	$\left rac{\overline{u_{6\xi}}}{U_0} ight $	1
Γ_{jx}	TJX	Jet thrust (can be measured directly in bollard pull condition)		N
n		Impeller rotation rate		Hz
n_i		Unit normal vector in <i>i</i> direction		1
$P_{\scriptscriptstyle m D}$		Delivered Power to pump impeller		W
$P_{ m E}$		Effective power:	$R_{\mathrm{TBH}}U_{0}$	W
$P_{ m JSE}$		Effective Jet System Power	$Q_{\scriptscriptstyle \mathrm{J}}H_{\scriptscriptstyle \mathrm{1A7}}$	W
$P_{ ext{PE}}$		Pump effective power:	$Q_{\mathrm{J}}H_{35}$	W
$P_{T\! ext{E}}$		Effective thrust power		W

TTC Symbol	Computer Symbol	Name	Definition or Explanation	SI- Unit
yiiiooi	Symbol	1	Explanation	Oilit
90	PR0	Ambient pressure in undisturbed flow		Pa
$p_{ m s}$		Local static pressure at station s		Pa
\overline{Q}		Impeller torque		Nm
		Volume flow rate inside boundary		m³/s
		Volume flow rate through water		
$Q_{\scriptscriptstyle m J}$		jet system		m^3/s
R_{TBH}		Total resistance of bare hull		N
$T_{\text{jet }x}$		Jet thrust (can be measured directly in bollard pull condition)		N
$T_{ m net}$		Net thrust exerted by the jet system on the hull		N
t		Thrust deduction fraction	$(1-t) = \frac{R_{\text{TBH}}}{T_{\text{net}}}$	1
$\overline{U_0}$		Free stream velocity		m/s
— U eis		Mean energy velocity in <i>i</i> direction at station s	$\sqrt{\frac{1}{Q_{\mathrm{J}}}\iint u_{\xi}^{3}dA}$	m/s
U es		Mean (total) energy velocity at station s	$\sqrt{\frac{1}{Q_{\rm J}} \iint u_{\xi}^{3} dA}$ $\sqrt{\frac{1}{Q_{\rm J}} \iint u^{3} dA}$	m/s
u_{is}		Velocity component in <i>i</i> -direction at station <i>s</i>		m/s
$u_{\rm s}$		Velocity at station s		m/s
$oldsymbol{l}_{7\phi}$	UJFI	Local tangential velocity at station 7		m/s
w_1		Geometric intake width at station 1		m
W_{1A}		Width of capture area measured over hull surface at station 1A		m
z_6		Vertical distance of nozzle centre relative to undisturbed surface		m
1 <i>M</i>	DMF	Change of momentum flux		N
$\Delta \overline{M}_x$		Change in Momentum Flux in <i>x</i> direction		N
$\eta_{\scriptscriptstyle m D}$		Overall propulsive efficiency:	$\frac{P_{\rm E}}{P_{ m D}}$	1
$\eta_{ ext{duct}}$		Ducting efficiency:	$\frac{P_{\text{JSE}}}{P_{\text{PE}}}$	1
$\eta_{ m eI}$		Energy interaction efficiency:	$rac{P_{ m JSE0}}{P_{ m JSE}}$	1
${oldsymbol{\eta}_{\scriptscriptstyle m I}}$		Ideal efficiency, equivalent to jet efficiency in free stream conditions	$rac{P_{ ext{TE0}}}{P_{ ext{JSE0}}}$	1
$\eta_{ ext{inst}}$		Installation efficiency to account for the distorted flow delivered by the jet intake to the pump		1

2.3.5 Water Jets

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ITTC	Computer	Name	Definition or	SI-
Symbol	Symbol	1	Explanation	Unit
$\eta_{ ext{INT}}$		Total interaction efficiency:	$\frac{\eta_{\rm eI}}{\eta_{\rm mI}} (1-t)$	1
$\eta_{ ext{jet}}$		Momentum or jet efficiency:	$rac{P_{ ext{TE}}}{P_{ ext{JSE}}}$	1
$\eta_{ exttt{JS}}$		Jet system efficiency:	$\frac{P_{ m JSE}}{P_{ m D}}$	1
$\eta_{ ext{mI}}$		Momentum interaction efficiency:	$\frac{T_{ m net0}}{T_{ m net}}$	1
$\eta_{_{ m P}}$	ETAP	Pump efficiency	$\frac{P_{\mathrm{PE}}}{P_{\mathrm{D}}}$	1
$\eta_{_{ m P0}}$		Pump efficiency from a pump loop test		1
$\eta_{_0}$		Free stream efficiency:	$\eta_{\scriptscriptstyle m P} \eta_{ m duct} \eta_{\scriptscriptstyle m I}$	1
θ_{n}		Jet angle relative to the horizontal at the nozzle (station 6)		rad
ρ		Mass density of fluid		kg/m³
ζ_{ij}		Energy loss coefficient between station <i>i</i> and <i>j</i>		1
ζ ₁₃	ZETA13	Inlet duct loss coefficient:	$\frac{E_{3} - E_{1}}{\frac{1}{2} \rho U_{0}^{2}}$ $\frac{E_{7} - E_{5}}{\frac{1}{2} - \frac{1}{2}}$	1
ζ ₅₇	ZETA57	Nozzle duct loss coefficient:	$\frac{E_7 - E_5}{\frac{1}{2} \rho u_{e6}}$	1

2.4.1 Manoeuvrability

D.C. W.

ITTC Computer Name Definition or SI-Symbol Symbol Explanation Unit

2.4 Manoeuvrability and Seakeeping

2.4.1 Manoeuvrability

2.4.1.1 Geometrical Quantities

see also Section 1.3.1 and Section 1.3.3

$A_{ m FB}$	AFBO	Projected area of bow fins		m^2
$A_{ m HL}$	AHLT	Lateral area of the hull	The area of the profile of the un- derwater hull of a ship when pro- jected normally upon the longitu- dinal centre plane	m ²
$A_{ m LV}$	AHLV	Lateral area of hull above water		m^2
$A_{\rm R}$	ARU	Total lateral area of rudder		m^2
$A_{ m Rmov}$	ARMV	Lateral area of movable part of rudder		m ²
$A_{ m RN}$	ARNO	Nominal lateral area of rudder	$(A_{\rm R} + A_{\rm Rmov}) / 2$	m^2
$b_{ m R}$	SPRU	Rudder span	Maximum distance from root to tip	m
$b_{ m RM}$	SPRUME	Mean span of rudder		m
C_{AL}	CAHL	Coefficient of lateral area of ship	$A_{\rm HL}$ / (L T)	1
h	DE	Water depth		m
$h_{ m M}$	DEME	Mean water depth		m
$x_{ m R}$	XRU	Longitudinal position of rudder axis		m
δ	ANRU	Rudder angle, helm angle		rad
$I_{\rm R}$	ASRU	Aspect ratio of rudder	$b_{\rm R}^2/A_{\rm R}$	1

2.4.1.2 Motions and Attitudes

2.4.1.2 N	Motions and Attitu	des		
p	OX, P	Roll velocity, rotational velocity about body <i>x</i> -axis		1/s
q	OY, Q	Pitch velocity, rotational velocity about body <i>y</i> -axis		1/s
r	OZ, R	Yaw velocity, rotational velocity about body <i>z</i> -axis		1/s
р	OXRT, PR	Roll acceleration, angular acceleration about body <i>x</i> -axis	dp / dt	$1/s^2$
\dot{q}	OYRT, QR	Pitch acceleration, angular acceleration about body <i>y</i> -axis	dq / dt	$1/s^2$
r	OZRT, RR	Yaw acceleration, angular acceleration about body <i>z</i> -axis	dr / dt	$1/s^2$
и	UX, U	Surge velocity, linear velocity along body <i>x</i> -axis		m/s
v	UY, V	Sway velocity, linear velocity along body <i>y</i> -axis		m/s
w	UZ, W	Heave velocity, linear velocity along body z-axis		m/s
ù	UXRT, UR	Surge acceleration, linear acceleration along body <i>x</i> -axis	du / dt	m/s ²
\dot{v}	UYRT, VR	Sway acceleration, linear acceleration along body <i>y</i> -axis	dv / dt	m/s ²
w	UZRT, WR	Heave acceleration, linear acceleration along body <i>z</i> -axis	dw / dt	m/s ²
V	V	Linear velocity of origin in body axes		m/s
$V_{\rm A}, V_0$	VA, V0	Approach speed		m/s
$V_{\rm u}$	V(URT)	Generalized velocity		m/s

2.4.1 Manoeuvrability

rad

rad

rad

see also section 3.4.2, Wind

ITTC	Computer	Name	Definition or	SI-
Symbol	Symbol	Name	Explanation	Unit
$\dot{V}_{_{ m u}}$	V(URT)	Generalized acceleration		m/s ²
$V_{ m F}$	VF	Flow or current velocity		m/s
$V_{ m WR}$	VWREL	Relative wind velocity		m/s
$V_{ m WT}$	VWABS	True wind velocity		m/s
Ψ	YA	Course angle or heading		rad
γ	YX	Yaw angle		rad
$d_{t\psi}$	YART	Rate of change of course	$d\psi / dt$	rad/s
$\Psi_{ m O}$	YA0R	Original course		rad
θ	PI	Pitch angle		rad
ϕ	RO	Roll angle		rad
.4.1.3 Flo	ow Angles etc.			
α	AAPI	Pitch angle	Angle of attack in pitch on the hull	rad
В	AADR	Drift angle	Angle of attack in yaw on the hull	rad
$eta_{ m WR}$	ANWIRL	Angle of attack of relative wind		rad
δ	ANCS	Angle of a control surface, rudder angle, helm angle		rad
δ_0	ANRU0	Neutral rudder angle		rad
$\delta_{ ext{EFF}}$	ANRUEF	Effective rudder inflow angle		rad
$\delta_{ ext{FB}}$	ANFB	Bow fin angle		rad
$\delta_{ ext{FS}}$	ANFS	Stern fin angle		rad
$\delta_{ m R}$	ANRU	Rudder angle		rad
$\delta_{ ext{RO}}$	ANRUOR	Rudder angle, ordered		rad
	COCII	C		1

Course of current velocity

Absolute wind direction

Relative wind direction

2.4.1.4 Forces and Derivatives

 $\psi_{\rm C}$

 ψ_{WA}

 $\psi_{
m WR}$

COCU

COWIAB

COWIRL

K	MX	Roll moment on body, moment		Nm
N IVIA	IVIA	about body <i>x</i> -axis		INIII
M	MY	Pitch moment on body, moment		Nm
IVI	101 1	about body <i>y</i> -axis		1 1111
N	MZ	Yaw moment on body, moment		Nm
1 V	IVIZ	about body z-axis		11111
$N_{ m r}$	NR	Derivative of yaw moment with	$\partial N / \partial r$	Nms
ı vr	IVIX	respect to yaw velocity	OIV / OI	111113
$N_{\dot{r}}$	NRRT	Derivative of yaw moment with	$\partial N / \partial \dot{\mathbf{r}}$	Nms^2
IV r	IVICICI	respect to yaw acceleration	011 / 01	111115
N_{ν}	NV	Derivative of yaw moment with	$\partial N / \partial v$	Ns
IVV	1 V V	respect to sway velocity	OIV / OV	113
$N_{\dot{v}}$	NVRT	Derivative of yaw moment with	$\partial N / \partial \dot{v}$	Nms ²
1 V V	IVVICI	respect to sway acceleration	011 / 01	111115
N_{δ}	ND	Derivative of yaw moment with	$\partial N / \partial \delta$	Nm
149	ND	respect to rudder angle	011 / 00	IVIII
Q_{FB}	QFB	Torque of bow fin		Nm
Q_{R}	QRU	Torque about rudder stock		Nm
Q_{FS}	QFS	Torque of stern fin		Nm
X	FX	Surge force on body, force along		N
Λ	$\Gamma\Lambda$	body x-axis		IN
X_{R}	XRU	Longitudinal rudder force		N
v	VII	Derivative of surge force with re-	$\partial X / \partial u$	NIa/:
X_u	XU	spect to surge velocity	UA / UU	Ns/m

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ITTC Symbol	Computer Symbol	Name	Definition or Explanation	SI- Unit
$X_{\dot{u}}$	XURT	Derivative of surge force with respect to surge acceleration	$\partial X / \partial \dot{u}$	Ns ² /m
Y	FY	Sway force, force in direction of body axis <i>y</i>		N
Y_r	YR	Derivative of sway force with respect to yaw velocity	$\partial Y / \partial r$	Ns
$Y_{\rm R}$	YRU	Transverse rudder force		N
$Y_{\dot{r}}$	YRRT	Derivative of sway force with respect to yaw acceleration	$\partial Y / \partial \dot{r}$	Ns^2
Y_{ν}	YV	Derivative of sway force with respect to sway velocity	∂Y / ∂v	Ns/m
$Y_{\dot{v}}$	YVRT	Derivative of sway force with respect to sway acceleration	$\partial Y / \partial \dot{v}$	Ns ² /m
Y_{δ}	YD	Derivative of sway force with respect to rudder angle	$\partial Y / \partial S$	N
Z	FZ	Heave force on body, force along body <i>z</i> -axis		N
	near Models			
C_r	CRDS	Directional stability criterion	$Y_{v}(N_{r}-mux_{G})-N_{v}(Y_{r}-mu)$	N^2s^2
$L_{ m b}$, $l_{ m b}$	LSB	Static stability lever	N_v / Y_v	m
$L_{ m d}$, $l_{ m d}$	LSR	Damping stability lever	$(N_r - mux_G) / (Y_r - mu)$	m
T	TIC	Time constant of the 1 st order manoeuvring equation		S
T_1	TIC1	First time constant of manoeuvring equation		S
T_2	TIC2	Second time constant of manoeuvring equation		S
T_3	TIC3	Third time constant of manoeuvring equation		S
K	KS	Gain factor in linear manoeuvring equation		1/s
P_n	PN	P-number, heading change per unit rudder angle in one ship length		1
	rning Circles			
$D_{\rm C}$	DC	Steady turning diameter		m
D_{C}	DCNO	Non-dimensional steady turning diameter	$D_{ m C}$ / $L_{ m PP}$	1
D_0	DC0	Inherent steady turning diameter $\delta_R = \delta_0$		m
D_0 '	DC0N	Non-dimensional inherent steady turning diameter	D_0 / $L_{ m PP}$	1
l_r	LHRD	Loop height of r - δ curve for unstable ship		rad/s
l_{δ}	LWRD	Loop width of r - δ curve for unstable ship		rad
$r_{\rm C}$	OZCI	Steady turning rate		1/s
r _C ′	OZCINO	Non-dimensional steady turning rate	$r_C L_{ m PP}$ / $U_{ m C}$ or 2 $L_{ m PP}$ / $D_{ m C}$	m
R_C	RCS	Steady turning radius		m
<i>t</i> ₉₀	TI90	Time to reach 90 degree change of heading		s
t_{180}	TI180	Time to reach 180 degree change of heading		s

Version 2021 2.4.1 Manoeuvrability

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ITTC	Computer	Name	Definition or	SI-
Symbol	Symbol	Name	Explanation	Unit
$U_{\rm C}$	UC	Speed in steady turn		m/s
x_{090}	X090	Advance at 90° change of heading		m
X ₀₁₈₀	X0180	Advance at 180° change of heading		m
$x_{0\text{max}}$	XMX	Maximum advance		m
Y 090	Y090	Transfer at 90° change of heading		m
\mathcal{Y}_{0180}	Y0180	Tactical diameter (transfer at 180° change of heading)		m
$\mathcal{Y}_{0 ext{max}}$	Y0MX	Maximum transfer		m
$eta_{ m C}$	DRCI	Drift angle at steady turning		rad
2.4.1.7 Ziş	g-Zag Manoeuvi	es		
$t_{\rm a}$	TIA	Initial turning time		S
t_{c1}	TIC1	First time to check yaw (starboard)		S
t_{c2}	TIC2	Second time to check yaw (port)		S
$t_{ m hc}$	TCHC	Period of changes in heading		S
$t_{ m r}$	TIR	Reach time		S
y_{0max}	Y0MX	Maximum transverse deviation		m
$\delta_{ ext{max}}$	ANRUMX	Maximum value of rudder angle		rad
$\psi_{ m S}$	PSIS	Switching value of course angle		rad
ψ_{01}	PSI01	First overshoot angle		rad
ψ_{02}	PSI02	Second overshoot angle		rad
2.4.1.8 Sto	opping Manoeuv	res		
$s_{ m F}$	SPF	Distance along track, track reach		m
$x_{0\mathrm{F}}$	X0F	Head reach		m
<i>y</i> _{0F}	Y0F	Lateral deviation		m
$t_{ m F}$	TIF	Stopping time		S

2.4.2 Seakeeping

D C '.'	CI	

ITTC	Computer	Nome	Definition or	SI-
Symbol	Symbol	Name	Explanation	Unit

2.4.2 Seakeeping

Related information is to be found in Chapter 3 on General Mechanics in Sections 3.1.2 on Time and Frequency Domain Quantities, 3.1.3 on Stochastic Processes, 3.2.1 on Inertial Properties,, 3.2.2 on Loads, 3.2.3 on Rigid Body Motions, and 3.4.1 on Waves.

2.4.2.1 Basic Quantities

	c Quantities		1	1 2
$A_{\mathrm{F}S}$	AFS	Projected area of stern fins		m ²
a_i	AT(I)	Attitudes of the floating system	i = 1, 2, 3, e.g. Euler angles of roll, pitch, and yaw, respectively	rad
r	FR	Frequency	1 / T	Hz
Ē	FE	Frequency of wave encounter	$1/T_{\rm E}$	Hz
? Z		Natural frequency of heave	$1/T_z$	Hz
θ		Natural frequency of pitch	$1/T_{\theta}$	Hz
r φ		Natural frequency of roll	$1/T_{\varphi}$	Hz
$F_{ m L}$	FS(2)	Wave excited lateral shear force	Alias horizontal!	N
F _N	FS(3)	Wave excited normal shear force	Alias vertical!	N
	MB(3),	Wave excited lateral bending mo-		
$M_{ m L}$	FS(6)	ment	Alias horizontal!	Nm
l <i>f</i>	MB(2),	Wave excited normal bending mo-	A1:	NI
$M_{ m N}$	FS(5)	ment	Alias vertical!	Nm
1.7	MT(1),	XX : 1, : 1		N.T.
$M_{ m T}$	FS(4)	Wave excited torsional moment		Nm
$\imath_{ m AW}$	NAW	Mean increased rate of revolution in waves		1/s
$P_{ m AW}$	PAW	Mean power increased in waves		W
$Q_{\rm AW}$	QAW	Mean torque increased in waves		Nm
		Mean resistance increased in		
$R_{ m AW}$	RAW	waves		N
$S_{\eta}(f), S_{\eta\eta}(f),$	EWSF,	Wave elevation auto spectral den-	see also section 1.4.1, Waves	m^2s
$S_{\eta}(\omega), S_{\eta\eta}(\omega)$	EWSC	sity	see also section 1.4.1, waves	111 8
	V(I)		i = 1, 2, 3 :surge, sway,	
x_i	X(I)		and heave respectively	m
χ_u	X(U)	Generalized displacement of a	u = 16 surge, sway, heave, roll,	m, rad
Nu .	Λ(0)	ship at the reference point	pitch, yaw	III, Iau
$T_{ m AW}$	TAW	Mean thrust increase in waves		N
Γ	TC	Wave period		S
$T_{\rm e}$	TE	Wave encounter period		S
$\frac{T_z}{T_{ heta}}$	TNHE	Natural period of heave		S
T_{θ}	TNPI	Natural period of pitch		S
T_{φ}	TNRO	Natural period of roll		S
$Y_z(\omega)$,		Amplitude of frequency response	$z_a(\omega)/\zeta_a(\omega)$ or	
$A_{z\zeta}(\omega)$		function for translatory motions	$z_a(\omega) / \eta_a(\omega)$	1
$Y_{\theta\zeta}(\omega)$,		Amplitude of frequency response	$\Theta_a(\omega) / \zeta_a(\omega)$ or	
$A_{ heta\zeta}(\omega)$,		function for rotary motions	$\Theta_a(\omega) / (\omega^2 / (g\zeta_a(\omega)))$	1
1		Tuning factor	$L_{z} = \frac{w_{E}}{w_{Z}} \qquad L_{q} = \frac{w_{E}}{w_{q}} \qquad L_{f} = \frac{w_{E}}{w_{f}}$ or	
u		Wave encounter angle	$L_z = \frac{T_z}{T_E} \qquad L_q = \frac{T_q}{T_E} \qquad L_f = \frac{T_f}{T_E}$ Angle between ship positive x axis and positive direction of waves (long crested) or dominant wave	rad
			direction (short crested)	

ITTC Symbols

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Ships in GeneralManoeuvrability and SeakeepingSeakeeping

ITTC	Computer	Nome	Definition or	SI-
Symbol	Symbol	Name	Explanation	Unit

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ITTC	Computer	Nama	Definition or	SI-
Symbol	Symbol	Name	Explanation	Unit

2.4.3 Large Amplitude Motions Capsizing Assumed centre of gravity above keel used for cross curves of stability - I99/1.2.4.1 Longitudinal centre of buoyancy Distance of centre of buoyancy from aft perpendicular -XAB ABm from aft perpendicular 199/1.2.4.2 Area of deck available to crew m^2 $A_{\rm C}$ Distance of the centre of flotation \overline{AF} XAF m from after perpendicular Longitudinal centre of gravity Distance of centre of gravity from $\overline{AG}_{\mathrm{L}}$ XAG m from aft perpendicular aft perpendicular Transverse distance from assumed centre of gravity A, to actual cen- AG_{T} YAG m tre of gravity G Vertical distance from assumed ZAG centre of gravity A, to actual cen- \overline{AG}_{V} m tre of gravity G AHLV Lateral area of hull above water m^2 $A_{
m LV}$ Positive area under righting lever A_{RL} m^2 $A_{\rm SI}$ Attained subdivision index ASI 1 I_{AS} Area of sails in profile according AS m² $A_{\rm S}$ to ISO 8666 Projected lateral area of the portion of the ship and deck cargo ΑV m² $A_{\rm V}$ above the waterline - IMO/IS, IMO/HSC'2000 Righting arm based on horizontal Generally tabulated in cross YAZdistance from assumed centre of m AZcurves of stability gravity A, to Z Centroid of the underwater vol-В Centre of buoyancy ume Breadth between centres of buoy- $B_{\rm CB}$ ancy of side hulls Distance from the centre of buoyancy CB to transverse metacentre Transverse metacentre above cen-ZBM BMtre of buoyancy $\overline{BM} = \frac{I_T}{\nabla} = \overline{KM} - \overline{KB}$ Longitudinal metacentre above $\overline{BM}_L = \overline{KM}_L - \overline{KB}$ **ZBML** m BM_L centre of buoyancy Centre of flotation of added buoyancy layer or centre of lost buoyancy of the flooded volume Maximum tank breadth m Proportion of boat plan needed for C_{D} Crew density crew Height coefficient, depending on the height above sea level of the C_H 1 structural member exposed to the

ITTC	Computer	Name	Definition or	SI-
Symbol	Symbol	1 (diffe	Explanation	Unit
			M'1	I
$C_{ m Lcpi}$		Crew limit	Maximum number of persons on board	
			Trimming moment divided by	
		Longitudinal trimming coefficient	change in trim which approxi-	
C_{MTL}	CMTL	- I99/1.2.4.3	mately equals	1
		1))/ 1.2.4.3	$\frac{1}{BM}L/L$	
		Shape coefficient, depending on	DIN L / L	
$C_{\rm s}$		the shape of the structural member		1
		exposed to the wind		
d	T	Draught, moulded, of ship hull -		m
a	1	I99/1.2.1		111
d		Density coefficient for submerged		1
		test weights Centre of flotation of the water		
F		plane		
F		Wind force - IMO/IS		
-		ma 10100 11110/110	From the freeboard markings to	
FREB	Freeboard	the freeboard deck, according to	m	
			official rules	
\overline{FB}	XFB	Longitudinal centre of buoyancy,	Distance of centre of buoyancy	m
ΓD		$L_{\rm CB}$, from forward perpendicular	from forward perpendicular	111
\overline{FF}	XFF	Longitudinal centre of flotation,	Distance of centre of floatation	m
		L_{CF} , from forward perpendicular Longitudinal centre of gravity,	from forward perpendicular Distance of centre of gravity from	
FG	XFG	from forward perpendicular	forward perpendicular	m
G		Centre of gravity of a vessel		
		Centre of gravity of an added or		1
g		removed weight (mass)		1
\overline{GG}_1	GGV	Vertical stability lever caused by a	$\overline{KG}_1 = \overline{KG}_0 + \overline{GG}_1$	m
001		weight shift or weight addition	KO1 - KO0 1 OO1	
\overline{CC}	GGH	Horizontal stability lever caused by a weight shift or weight addi-		m
$GG_{ m H}$	GGII	tion		m
		Longitudinal stability lever caused		
$\overline{GG}_{\mathrm{L}}$	GGL	by a weight shift or weight addi-		m
		tion		
$\overline{GG}_{ m V}$	GGV	Vertical stability lever caused by a	$\overline{KG}_1 = \overline{KG}_0 + \overline{GG}_1$	m
301		weight shift or weight addition	·	
			Distance of centre of gravity to the metacentre	
\overline{GM}	GM	Transverse metacentric height	$\frac{\overline{GM} = \overline{KM} - \overline{KG}}{\overline{GM}}$	m
G/WI	GW	Transverse metacentric height	GM = KM - KG (not corrected for free surface ef-	111
			fect)	
		Effective transverse metacentric		
$\overline{GM}_{ ext{EFF}}$	GMEFF	height	GM Corrected for free surface and/or free communication effects	m
			Distance from the centre of gravity	
			G to the longitudinal metacentre	
$\overline{GM_L}$	GML	Longitudinal metacentric height	$M_{ m L}$	m
L			$\overline{GM}_L = \overline{KM}_L - \overline{KG}$	
${C7}$	GZ	Righting arm or lever	$GZ = AZ - AG_{\rm V} \sin \varphi -$	m
GZ	UL	Argumg and of level	$\overline{AG}_{T} \cos \varphi$	m
			110 1 003 ψ	ļ

Nm

kg

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 $M_{\rm FS}$

 $m_{\rm LCC}$

ITTC Computer Definition or SI-Name Symbol Symbol Explanation Unit Arm of static stability corrected \overline{GZ} m for free surfaces - IMO/table **GZMAX** Maximum righting arm or lever m GZ_{MAX} Maximum tank height m Height of centre of area of A_{SP} $h_{\rm CE}$ m above waterline at SSM Heeling lever (due to various rea-HLm sons) - IMO/HSC'2000 Height of waterline above centre h_{LP} m of area of immersed profile Keel reference Distance from the assumed centre Assumed centre of gravity above \overline{KA} ZKA of gravity A to the moulded base m moulded base of keel of keel or K Distance from the centre of buoy-Centre of buoyancy above ZKB ancy B to the moulded base of keel m \overline{KB} moulded base of keel Centre of gravity above moulded Distance from the centre of gravity ZKG \overline{KG} m base of keel G to the moulded base of keel or K Vertical centre of gravity of added Distance from the assumed centre of gravity, g, to the moulded base KgZKAG or removed weight above moulded m base of keel of keel or K Distance from the transverse meta-Transverse metacentre above $\overline{K}M$ ZKM centre M to the moulded base of m moulded base of keel keel or K Distance from the longitudinal Longitudinal metacentre above $\overline{KM}_{\mathrm{L}}$ ZKML metacentre $M_{\rm L}$ to the moulded m moulded base of keel base of keel or K Roll damping coefficient express-1 ing the effect of bilge keels Length of the vessel on the waterline in maximum load condition -L m IMO/IS Arm of dynamic stability corrected for free surfaces m IMO/table $X_{\rm CG} - X_{\rm CB}$ XTA Longitudinal trimming arm m Maximum tank length m Actual length of enclosed superstructure extending from side to m side of the vessel Wind heeling lever m M Metacentre of a vessel See subscripts for qualification SHIPMA Ship mass W/gkg m Maximum offset load moment due Nm $M_{\rm C}$ Minimum capsizing moment as determined when account is taken $M_{\rm c}$ Nm Free surface moment at any incli-

nation

Mass in light craft condition

Ships in General Manoeuvrability and Seakeeping Large Amplitude Motions Capsizing

ITTC	Computer	Name	Definition or	SI-
Symbol	Symbol		Explanation	Unit
		Mass in loaded displacement con-		
$m_{ m LDC}$		dition according to		kg
Ma cox		Maximum total load (mass)		kg
$m_{ m MTL}$ $M_{ m R}$		Heeling moment due to turning		Nm
<i>IVI</i> R		Heeling moment due to turning		INIII
$M_{ m S}$	MS	Moment of ship stability in general	ΔGZ . Other moments such as those of capsizing, heeling, etc. will be represented by M_S with additional subscripts as appropriate.	Nm
700		Mass in standard sailing condi-		lea.
$m_{\rm SSC}$		tions according to		kg
$M_{T{ m C}}$	MTC	Moment to change trim one centimetre	metre	
$M_{T m M}$	MTM	Moment to change trim one meter	ΔC_{MTL}	Nm/m
$M_{ m W}$		Maximum heeling moment due to wind		Nm
$M_{ m v}$		Dynamically applied heeling moment due to wind pressure		Nm
\overline{OG}		Height of centre of gravity above waterline		m
$P_{ m V}$		Wind pressure		Pa
r		Effective wave slope coefficient		1
$R_{\rm SI}$	RSI	Required subdivision index		1
S	11.01	Wave steepness		1
STIX	STIX	Actual stability index value according to		1
STIX	STIXR	Required stability index value, see		1
T	YHA	Equivalent transverse heeling arm	Heeling moment/∆	m
TL		Turning lever	5	m
$t_{ m s} \ t_{ m KL}$	TRIM	Static trim	$T_{\rm A}$ - $T_{\rm F}$ - $d_{\rm KL}$	m
V v		Tank total capacity		m³
V_0		Speed of craft in the turn - IMO/HSC'2000 Service speed - IMO/IS		m/s
$v_{ m W}$		Wind speed used in calculation		m/s
W	SHIPWT	Ship weight	m g	N
x_{CB}	XACB	Longitudinal centre of floatation of added buoyant layer	Longitudinal distance from reference point to the centre of the added buoyant layer, b	m
X_{CB} L_{CB}	XCB	Longitudinal centre of buoyancy (L_{CB})	Longitudinal distance from reference point to the centre of buoyancy, B	m
X_{CF} L_{CF}	XCF	Longitudinal centre of flotation (L_{CF})	Longitudinal distance from reference point to the centre of flotation, F	m
$x_{\rm CG}$	XACG	Longitudinal centre of gravity of added weight (mass)	Longitudinal distance from reference point to the centre of gravity, g, of an added or removed weight (mass)	m

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ITTC	Computer	Name	Definition or	SI-
Symbol	Symbol	runic	Explanation	Unit
	1		I	1
$X_{\rm CG}$	WOO	Longitudinal centre of gravity	Longitudinal distance from refer-	
$L_{ m CG}$	XCG	(L_{CG})	ence point to the centre of gravity,	m
		` ′	G	1
X_1, X_2		Roll damping coefficients		1
x_{D}		Distance of down flooding open-		m
Y_{CG}		ing from end of boat Lateral displacement of centre of	Lateral distance from a reference	
,	YCG	gravity (Y_{CG})	point to the centre of gravity, G	m
<i>y</i> cg		Distance of down flooding open-	point to the centre of gravity, G	
y_{D}		ing from gunwale		m
		Distance of down flooding open-		
y_{D}'		ing off centreline		m
		Intersection of righting arm with		
Z	ZRA	line of action of the centre of		
		buoyancy		
		Vertical distance from the centre		
		of A to the centre of the underwa-		
Z		ter lateral area or approximately to		m
		a point at one half the draught -		
		IMO/IS		
Z, h		Vertical distance from the centre		m
<i>L</i> , <i>n</i>		of A to the waterline		111
$z_{ m D}$		Height above waterline of down		m
<u></u>		flooding opening		
ZSA	ZSA	Static sinkage at AP	Caused by loading	m
ZSF	ZSF	Static sinkage at FP	Caused by loading	m
ZS	ZS	Mean static sinkage	$(z_{SF}+z_{SA})/2$	m
δ		Tank block coefficient		1
$\delta t_{ m KL}$	DTR	Change in static trim		m
Δ	DISPF	Displacement (buoyant) force	$g \rho \nabla$	N
Δ_m	DISPM	Displacement mass	ρ ∇	kg
∇	DISPVOL	Displacement volume	$\Delta/(\rho g)$	m³
$V_{ m fw}$	DISVOLFW	Displacement volume of flooded	$\Delta_{ m fw}$ / $(ho m g)$	m^3
r IW	DIS VOLI VI	water	Δ_{IW} , (pg)	***
ϕ	HEELANG	Heel angle		rad
\$\phi_0		Heel angle during offset load tests		rad
$\phi_{0(\text{REQ})}$		Maximum permitted heel angle		rad
YV(KEQ)		during		
$\phi_{ m D}$		Actual down flooding angle ac-		rad
, =		cording to		
$\phi_{\mathrm{D(REQ)}}$		Required down flooding angle,		rad
		See		1
$\phi_{ m DC}$		Down flooding angle to non-quick draining cockpits		rad
		Down flooding angle to any main		
$\phi_{ m DH}$		access hatchway		rad
$\phi_{ m F}$	HEELANGF	Heel angle at flooding		rad
ψ_{Γ}	IILLLANGI	Angle of heel at which maximum		ıau
				rad
ϕ_{GZMAX}		irioniino momeni occurs		1
		righting moment occurs Assumed roll angle in a seaway		rad
ϕ_{GZMAX} ϕ_{R} ϕ_{VS}	HEELANGV	Assumed roll angle in a seaway Heel angle for vanishing stability		rad rad

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Version 2021

ITTC	Computer	Name	Definition or	SI-
Symbol	Symbol	Name	Explanation	Unit
			The ratio of the volume of flood-	
μ	PMVO	Volumetric permeability	ing water in a compartment to the	1
			total volume of the compartment	
$\theta_{ m c}$		Capsizing angle under the action		rad
$O_{\rm c}$		of a gust of wind IMO/IS		rau
		Heel angle corresponding to the		
$\phi_{ m m}$		maximum of the statical stability		rad
		curve		
$\theta_{\rm S}$	TRIMS	Static trim angle	$\tan^{-1}((z_{SF}-z_{SA})/L)$	rad
ρ	RHO	(Liquid) mass density		kg/m³
	RHOA	(Air) mass dansity		1r.cv/ma3
$ ho_{\mathrm{A}}$	DNA	(Air) mass density		kg/m³
$ ho$ \otimes	DNWA	(Water) mass density		kg/m³

2.4.4 Symbols for Attributes and Subscripts

A	Aft
E	Entrance
F	Fore
R	Run
Z	Heave
θ	Pitch
φ	Roll

ITTC Symbols

3 **Special Craft**

3.1 Planing and Semi-Displacement Vessels

Geometry and Hydrostatics Version 2021 3.1.1

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ITTC	Computer	Name	Definition or	SI-
Symbol	Symbol	Name	Explanation	Unit

SPECIAL CRAFT 3.

3.1

3.1.1

Planing and Semi-Displacement Vessels
Geometry and Hydrostatics
See also Section 1.2.1, Hull Geometry and Section 1.2.2 Propulsor Geometry

	ce diso section 1.2.1	1, Truit Geometry and Section 1.2.2 Propi		
$A_{ m P}$	APB	Planing bottom area	Horizontally projected planing bottom area (at rest), excluding area of external spray strips	m^2
$B_{L{ m CG}}$	BLCG	Breadth at longitudinal position of the centre of gravity	Breadth over spray strips measured at transverse section containing centre of gravity	m
$B_{ m PC}$	BPC	Breadth over chines	Breadth over chines, excluding external spray strips	m
B_{PA}	BPA	Mean breadth over chines	$A_{ m P}$ / $L_{ m P}$	m
$B_{ m PT}$	BPT	Transom breadth Breadth over chines at transom, excluding external spray strips		m
$B_{ m PX}$	BPX	Maximum breadth over chines	Maximum breadth over chines, ex- cluding external spray strips	m
L_{SB}	LSB	Total length of shafts and bossings		m
$L_{ m PR}$	LPRC	Projected chine length	Length of chine projected in a plane parallel to keel	m
β	BETD	Deadrise angle of planing bottom	Angle between a straight line approximating body section and the intersection between basis plane and section plane	rad
$\beta_{ m M}$	BETM	Deadrise angle at midship section	_	rad
$oldsymbol{eta_{ ext{T}}}$	BETT	Deadrise angle at transom		rad
$arepsilon_{ ext{SH}}$	EPSSH	Shaft angle	Angle between shaft line and ref- erence line (positive, shaft inclined downwards)	rad

ITTC	Computer	Nama	Definition or	SI-
Symbol	Symbol	Name	Explanation	Unit

3.1.2 Geometry and Levers, Underway 3.1.2.1 Geometry, Underway

3.1.2.1 Ge	cometry, Underw	ay		
$d_{ m TR}$	DTRA	Immersion of transom, underway	Vertical depth of trailing edge of boat at keel below water surface level	m
$h_{ m P}$	HSP	Wetted height of strut palms (flange mounting)		m
$h_{ m R}$	HRU	Wetted height of rudders		m
$L_{\rm C}$	LC	Wetted chine length, underway		m
l_{CP}	LCP	Lever of resultant of pressure forces, underway	Distance between centre of pressure and aft end of planing surface	m
L_{K}	LK	Wetted keel length, underway		m
$L_{ m M}$	LM	Mean wetted length, underway	$(L_{\rm K} + L_{\rm C}) / 2$	m
$S_{ m WHP}$	Wetted area underway of planing Principal wetted area boun		Principal wetted area bounded by trailing edge, chines and spray	m^2
$S_{ m WB}$	SWB Wetted bottom area, underway Area bounded by stagnation line, chines or water surface underway and transom		m ²	
$S_{ m WHE}$	SWHE Wetted hull area, underway Total wetted derway, incl wetted side a		Total wetted surface of hull un- derway, including spray area and wetted side area, w/o wetted tran- som area	m^2
$S_{ m WHS}$	SWSH	Area of wetted sides Wetted area of the hull side above the chine or the design water line		m ²
$S_{ m WS}$, $S_{ m S}$	SWS	Area wetted by spray Wetted area between design l or stagnation line and spray e		m^2
$lpha_{ m B}$	ALFSL	Angle of stagnation line	Angle between projected keel and stagnation line in a in plane normal to centre plane and parallel to reference line	rad
$lpha_{ m BAR}$	ALFBAR	Barrel flow angle	Angle between barrel axis and assumed flow lines	rad
$arepsilon_{\mathrm{W}L}$	EPSWL	Wetted length factor	$L_{ m M}$ / $L_{ m WL}$	1
$\varepsilon_{\mathrm{W}S}$	EPSWS	Wetted surface area factor	S/S_0	1
$ heta_{ m DWL},$	TRIMDWL	Running trim angle based on design waterline	Angle between design waterline and running waterline (positive bow up)	rad
$ heta_{ m S},~ heta_0$	TRIMS	Static trim angle	Angle between ship design water- line and actual water line at rest (positive bow up) $\tan^{-1}((z_{SF} - z_{SA})/L)$	rad
$ heta_V$, $ heta_{ m D}$	TRIMV	Running (dynamic) trim angle	Angle between actual water line at rest and running water line (positive bow up) $tan^{-1}((z_{VF} - z_{VA})/L)$	rad
$\lambda_{ m W}$	LAMS	Mean wetted length-breadth ratio	$L_{\rm M}$ / ($B_{\rm LCG}$)	1
τ	TRIMDWL	Running trim angle based on design waterline	Angle between design waterline and running waterline (positive bow up)	deg
$ au_{ m DWL}$	TAUDWL	Reference line angle	Angle between the reference line and the design waterline	rad
$ au_{ m R}$	TAUR	Angle of attack relative to the reference line	Angle between the reference line and the running waterline	rad

FRT

Distance between R_T and centre of

gravity (measured normal to R_T)

3.1.2 Geometry and Levers, Underway

ITTC Computer Definition or SI-Name Symbol Symbol Explanation Unit Angle between stagnation line and PHISP Spray angle rad $\varphi_{\rm SP}$ keel (measured in plane of bottom) Effective increase in friction area Dimensionless increase in total δ_{λ} **DLAM** length-breadth ratio due to spray friction area contribution to drag 3.1.2.2 Levers, Underway Distance between N_A and centre of ENAPP Lever of appendage lift force N_A $e_{\rm A}$ gravity (measured normally to N_A) Distance between $N_{\rm B}$ and centre of **ENBOT** Lever of bottom normal force $N_{\rm B}$ e_{B} m gravity (measured normally to $N_{\rm B}$) Distance between propeller centre-Lever of propeller normal force **ENPN** line and centre of gravity (measm e_{PN} ured along shaft line) Distance between N_{PP} and centre Lever of resultant of propeller **ENPP** e_{PP} of gravity (measured normally to m pressure forces N_{PP} Distance between N_{PS} and centre Lever of resultant propeller suc-**ENPS** of gravity (measured normal to m e_{PS} tion forces N_{PS} $N_{\rm PS}$) Distance between N_{RP} and centre Lever of resultant of rudder pres-ENRP of gravity (measured normal to m e_{RP} sure forces N_{RP} Distance between R_{AA} and centre f_{AA} FRAA Lever of wind resistance R_{AA} of gravity (measured normal to m $R_{\rm AA}$) Distance between R_{AP} and centre FRAP of gravity (measured normal to Lever of appendage drag R_{AP} $f_{\rm AP}$ m Distance between R_F and centre of $f_{\rm F}$ FRF Lever of frictional resistance $R_{\rm F}$ gravity (measured normal to $R_{\rm F}$) Distance between $R_{\rm K}$ and centre of FRK Lever of skeg or keel resistance $R_{\rm K}$ $f_{\rm K}$ m gravity (measured normal to $R_{\rm K}$) Distance between ΔR_{RP} and centre Lever of augmented rudder drag $f_{\rm R}$ FDRR of gravity (measured normal to m $\Delta R_{\rm RP}$) Distance between axial thrust and FSL Lever of axial propeller thrust centre of gravity (measured norm $f_{\rm S}$ mal to shaft line)

Lever of total resistance R_T

ITTC	Computer	Nome	Definition or	SI-
Symbol	Symbol	Name	Explanation	Unit

3.1.3 Resistance and Propulsion

C_{L0}	CL0D	1 on Hull Resistance Lift coefficient for zero deadrise	$\Delta / (B_{\rm CG}^2 q)$	1
CLβ	CLBET	Lift coefficient for deadrise sur- face	$\Delta / (B_{\rm CG}^2 q)$	1
C_V	CSP	Froude number based on breadth	$V/(B_{\rm CG}g)^{1/2}$	1
7 7	CDL	Load coefficient	$\Delta / (B_{\rm CG}^3 \rho g)$	1
VHD	LVD	Vertical component of hydrody- namic lift	, , ,	N
VS	LVS	Hydrostatic lift	Due to buoyancy	N
TA	FTAPP	Appendage drag force (parallel to reference line)	Drag forces arising from appendages inclined to flow, assumed to act parallel to the reference line	N
⁷ тв	FTBOT	Bottom frictional force (parallel to reference line)	Viscous component of bottom drag forces assumed acting paral- lel to the reference line	N
Ттк	FTKL	Keel or skeg drag force (parallel to reference line)	Drag forces arising from keel or skeg, assumed to act parallel to the reference line	N
TTRP	FTRP	Additional rudder drag force (par- allel to reference line)	Drag forces arising from influence of propeller wake on the rudder assumed to act parallel to the ref- erence line	N
V_{A}	NAPP	Appendage lift force (normal to reference line)	Lift forces arising from appendages inclined to flow, assumed to act normally to reference line	N
$V_{ m B}$	NBOT	Bottom normal force (normal to reference line)	Resultant of pressure and buoyant forces assumed acting normally to the reference line	N
$V_{P\mathtt{P}}$	NPP	Propeller pressure force (normal to		N
V_{PS}	NPS	Propeller suction force (normal to reference line)	Resultant of propeller suction forces acting normally to the reference line	N
$V_{ m RP}$	NRP	Rudder pressure force (normal to reference line)	Resultant of rudder pressure forces acting normally to the reference line	N
$R_{\rm K}$	RKEEL	Keel drag		N
R_{π}	RPI	Induced drag	$g \rho V tan \tau$	N
$R_{\rm PAR}$	RPAR	Parasitic drag	Drag due to inlet and outlet openings	N
R_{PS}	RSP	Pressure component of spray drag		N
₹ _T	RT	Total resistance	Total towed resistance	N
$R_{ m VS}$	RSV	Viscous component of spray drag	$C_{\rm F} S_{ m WS} q_{ m S}$	N
ВМ	VBM	Mean bottom velocity	Mean velocity over bottom of the hull	m/s
$V_{ m SP}$	VSP	Spray velocity	Relative velocity between hull and spray in direction of the spray	m/s

3.2 Multi-Hull Vessels3.2.1 Geometry and Hydrostatics

ITTC	Computer	Nama	Definition or	SI-
Symbol	Symbol	Name	Explanation	Unit

3.2 Multi-Hull Vessels

3.2.1 Geometry and Hydrostatics See also Section 2.2.1, Hull Geometry

	ee also Section 2.2.1,			1 2
$A_{\rm I}$	AIA	Strut-hull intersection area		m ²
B_{B}	BB	Box breadth	Breadth of main deck	m
B_{S}	BS	Hull spacing	Distance between hull centre lines	m
$B_{ m TV}$	BTUN	Tunnel width	Minimal distance of the demihulls at the waterline	m
$D_{ m H}$	DHUL	Hull diameter	Diameter of axis symmetric sub- merged hulls	m
D_{X}	DX	Hull diameter at the longitudinal position "X"		m
$H_{ m DK}$	HCLDK	Deck clearance	Deck clearance Minimum clearance of wet deck from water surface at rest	
$H_{\rm SS}$	HSS	Strut submerged depth	Depth of strut from still water line to strut-hull intersection	m
$i_{ m EI}$	ANENIN	Half angle of entrance at tunnel (inner) side Angle of inner water line with reference to centre line of demihull		rad
$i_{ m EO}$	ANENOU	Half angle of entrance at outer side	Angle of outer water line with reference to centre line of demihull	rad
L_{CH}	LCH	Length of centre section of hull	Length of prismatic part of hull	m
$L_{\rm CS}$	LCS	Length of centre section of strut	Length of prismatic part of strut	m
$L_{ m H}$	LH	Box length	Length of main deck	m
$L_{ m NH}$	LNH	Length of nose section of hull	Length of nose section of hull with variable diameter	m
$L_{ m NS}$	LNS	Length of nose section of strut	Length of nose section of strut with variable thickness	m
$L_{ m S}$	LS	Strut length	Length of strut from leading to trailing edge	m
L_{SH}	LSH	Length of submerged hull		m
$t_{ m S}$	TSTR	Maximum thickness of strut		m

3.2.2 Resistance and Propulsion Version 2021

ITTC	Computer	Nome	Definition or	SI-
Symbol	Symbol	Name	Explanation	Unit

3.2.2 Resistance and Propulsion

3.2.2.1 Resistance Components See also Section 2.3.1 on Hull Resistance

50	ce also beetion 2.5.	1 On Thin Resistance		
$R_{ m FMH}$	RFMH	Frictional resistance of multi-hull vessel		N
$R_{ m FINT}$	RFINT	Frictional resistance interference correction	$R_{ m FMH}$ - Σ $R_{ m F}$	N
$R_{ m RMH}$	RRMH	Residuary resistance correction of multi-hull	$R_{ m TMH}$ - $R_{ m FMH}$	N
$R_{ m RI}$	RRINT	Residuary resistance interference correction	$R_{ m RMH}$ - $\Sigma R_{ m R}$	N
R_{TMH}	RTMH	Total resistance of multi-hull ves- sel		N
R_{TI}	RTINT	Total resistance interference cor- rection	R_{TMH} - ΣR_{T}	N

ITTC

Symbol

3.3 Hydrofoil Boats3.3.1 Geometry and Hydrostatics

Definition or	SI-
Explanation	Unit

3.3 Hydrofoil Boats

3.3.1 Geometry and Hydrostatics See Sections 2.2.1 and 2.2.4

Computer

Symbol

Name

A_{F}	AFO	Foil area (general)	Foil area in horizontal plane	m^2
$A_{ m FT}$	AFT	Total foil plane area		m ²
$B_{ m FOA}$	BFOA	Maximum vessel breadth including foils		m
$b_{ m S}$	BST	Span of struts		m
$b_{ m ST}$	BSTT	Transverse horizontal distance of struts		m
c_{C}	СНС	Chord length at centre plane		m
$c_{ m F}$	CFL	Chord length of flap		m
$c_{ m M}$	CHM	Mean chord length		m
c_{S}	CSTR	Chord length of a strut		m
$\mathcal{C}_{\mathrm{SF}}$	CHSF	Chord length of strut at intersection with foil		m
CT	CHTI	Chord length at foil tips		m
W_{F}	WTF	Weight of foil		N
$\alpha_{\rm c}$	ALFTW	Geometric angle of twist		rad
$\theta_{ m DH}$	DIHED	Dihedral angle		rad
$\overline{V_{ m F}}$	DISVF	Foil displacement volume		m^3

<u>3.3.1.1 C</u>	šeometry, Under			
$A_{ m FE}$	AFE	Emerged area of foil		m^2
$A_{ m FF}$	ASFF	Submerged area of front foil		m^2
$A_{ m FR}$	ASFR	Submerged area of rear foil		m^2
$A_{\mathrm FS}$	AFS	Submerged foil area		m^2
$A_{ m FST0}$	AFSTO	Submerged foil plan area at take- off speed		m^2
A_{SS}	ASS	Submerged strut area		m^2
$b_{ m w}$	BSPW	Foil span wetted		m
$\mathcal{C}_{P\mathrm{F}}$	CPFL	Distance of centre of pressure on a foil or flap from leading edge		m
Fr_L	FNFD	Froude number based on foil distance	$V/(gL_{ m F})^{1/2}$	1
Fr_c	FNC	Froude number based on chord length	$V/(g c_{\rm M})^{1/2}$	1
h_{CG}	HVCG	Height of centre of gravity foil- borne	Distance of centre of gravity above mean water surface	m
$h_{ m F}$	HFL	Flight height	Height of foil chord at foilborne mode above position at rest	m
$h_{ m K}$	НКЕ	Keel clearance	Distance between keel and mean water surface foilborne	m
l_{F}	LEFF	Horizontal distance of centre of pressure of front foil to centre of gravity		m
$l_{ m FR}$	LEFR	Horizontal distance between cen- tres of pressure of front and rear foils	$l_{ m F}+l_{ m R}$	m
$l_{ m R}$	LERF	Horizontal distance of centre of pressure of rear foil to centre of gravity		m
$T_{ m F}$	TFO	Foil immersion	Distance between foil chord and mean water surface	m

3.3 Hydrofoil Boats3.3.1 Geometry and Hydrostatics

ITTC Symbol	Computer Symbol	Name	Definition or Explanation	SI- Unit
$T_{ m FD}$	TFD	Depth of submergence of apex of a dihedral foil	Distance between foil apex and mean water surface	m
$T_{ m FM}$	TFOM	Mean depth of foil submergence		m
$a_{ ext{IND}}$	ALFIND	Downwash or induced angle		rad
$a_{ m M}$	ALFM	Angle of attack of mean lift coefficient for foils with twist		rad
$a_{ m s}$	AFS	Angle of attack for which flow separation (stall) occurs		rad
$\alpha_{ ext{TO}}$	ATO	Incidence angle at take-off speed		rad

3.3 Hydrofoil Boats 3.3.2 Resistance and Propulsion

ITTC	Computer	Nome	Definition or	SI-
Symbol	Symbol	Name	Explanation	Unit

3.3.2 Resistance and Propulsion See also Section 2.3.1 Hull Resistance

3.3.2.1 Basic Quantities

$D_{ m F}$	DRF	Foil drag	Force in the direction of motion of	N
D_{F}	Ditt	1 on drag	an immersed foil	14
D_{FR}	DFA	Drag force on rear foil	$C_{DF} A_{FR} q$	N
$D_{ m FF}$	DFF	Drag force on front foil	$C_{DF}A_{FF}q$	N
$D_{\rm I}$	DRIND	Induced drag	For finite span foil, the component of lift in the direction of motion	N
$D_{ m INT}$	DRINT	Interference drag	Due to mutual interaction of the boundary layers of intersecting foil	N
$D_{ m P0}$	DRF0	Profile drag for angle of attack equal to zero lift	Streamline drag	N
D_{S}	DRSP	Spray drag	Due to spray generation	N
D_{ST}	DRST	Strut drag		N
D_{W}	DRWA	Wave drag	Due to propagation of surface waves	N
$D_{ m V}$	DRVNT	Ventilation drag	Due to reduced pressure at the rear side of the strut base	N
L_{F}	LF	Lift force on foil	$C_L A_{\rm FT} q$	N
$L_{ m FF}$	LFF	Lift force on front foil	$C_L A_{\rm FF} q$	N
L_{FR}	LFR	Lift force on rear foil	$C_L A_{\rm FR} q$	N
L_0	LF0	Profile lift force for angle of attack of zero		N
L_{TO}	LT0	Lift force at take off	$C_{L{ m TO}}A_{{ m FT}}q$	N
M	MSP	Vessel pitching moment		Nm

 $M_{\rm R}$

MLR

EPSLDF

3.3 Hydrofoil Boats 3.3.2 Resistance and Propulsion

 $L_{\rm FR}/\Delta$

L/D

ITTC	Computer	Ni	Definition or	SI-
Symbol	Symbol	Name	Explanation	Unit
3.3.2.2 De	erived Quantities	S		
C_{DF}	CDF	Drag coefficient of foil	$D_{\rm F}$ / $(A_{\rm FS} q)$	1
C_{DI}	CDI	Induced drag coefficient	$D_{\rm I}$ / $(A_{\rm FS} q)$	1
C_{DINT}	CDINT	Interference drag coefficient	$D_{\mathrm{INT}} / (A_{\mathrm{FS}} q)$	1
C_{D0}	CDO	Section drag coefficient for angle of attack equal to zero	$D_{ m P} / (A_{ m FS} q)$	1
$C_{D\mathrm{S}}$	CDSP	Spray drag coefficient	$D_{\rm S}$ / $(A_{\rm FS} q)$	1
$C_{D{ m VENT}}$	CDVENT	Ventilation drag coefficient	$D_{ m V}/\left(A_{ m FS}q ight)$	1
$C_{D\mathrm{W}}$	CDW	Wave drag coefficient	D_{W} / $(A_{\mathrm{FS}} q)$	1
$C_{L{ m F}}$	CLF	Foil lift coefficient	$L_{\rm F}$ / $(A_{\rm FS} q)$	1
C_{L0}	CLO	Profile lift coefficient for angle of attack equal to zero	$L_0 / (A_{ m FS} q)$	1
$C_{L{ m TO}}$	CLTO	Lift coefficient at take-off condition	$L_{ m TO}$ / $(A_{ m FS} q)$	1
C_{LX}	CLA	Slope of lift curve	$dC_L/d\alpha$	1
C_M	CM	Pitching moment coefficient	$M/((A_{\mathrm{FF}}+A_{\mathrm{FR}})(l_{\mathrm{F}}-l_{\mathrm{R}})q)$	1
$M_{ m F}$	MLF	Load factor of front foil	$L_{ ext{FF}}$ / Δ	1
1.6	MID	T 1 C + C C '1	T / A	1

Load factor of rear foil

Lift/ Drag ratio of foil

3.4 ACV and SES 3.4.1 Geometry and Hydrostatics

ITTC	Computer	Nome	Definition or	SI-
Symbol	Symbol	Name	Explanation	Unit

3.4 ACV and SES

3.4.1 Geometry and Hydrostatics See also Section 1.2.1

also beetion 1.2.1			
CUA	Cushion area	cushion on water surface	m^2
BCU	Cushion breadth	SES cushion breadth measured between the side walls	m
BWLT	Total waterline breadth of SES	At the water line	m
HVCG	Height of centre of gravity above mean water plane beneath craft		m
HBS	Bow seal height	Distance from side wall keel to lower edge of bow seal	m
HSK	Skirt depth		m
HSS	Stern seal height	Distance from side wall keel to lower edge of stern seal	m
LB	Deformed bag contact length		m
LAC	Cushion length		m
LACE	Effective length of cushion	$A_{\rm C}/B_{\rm C}$	m
SSH0	Wetted area of side hulls at rest off cushion		m^2
SSHC	Wetted area of side hulls under way on cushion	Total wetted area of side walls un-	m^2
SSH	Wetted area of side hulls under way off cushion	Total wetted area of side walls un- der way off cushion	m ²
XH, LH	Horizontal spacing between inner and outer side skirt hinges or at- tachment points to structure	needs clarification	m
XS, LS	Distance of leading skirt contact point out-board or outer hinge of attachment point to structure	needs clarification	m
ZH, HH	Vertical spacing between inner and outer side skirt hinges or at- tachment points to structure	needs clarification	m
DBCV	Increase in cushion breadth due to water contact		m
EPSWS	Wetted surface factor	$S_{ m SHC}$ / $S_{ m SH0}$	1
TETB	Bag contact deformation angle		rad
TETF	Finger outer face angle		rad
TETW	Slope of mean water plane for sur- face level beneath cushion periph- ery		rad
DNA	(ACV and SES) Mass density of air	Mass of air per unit volume	kg/m ³
ZETAC	Height of cushion generated wave above mean water plane at leading edge side of the skirt		m
	BCU BWLT HVCG HBS HSK HSS LB LAC LACE SSHO SSHC SSH XH, LH XS, LS ZH, HH DBCV EPSWS TETB TETF TETW DNA	BCU Cushion breadth BWLT Total waterline breadth of SES Height of centre of gravity above mean water plane beneath craft HBS Bow seal height HSK Skirt depth HSS Stern seal height LB Deformed bag contact length LAC Cushion length LACE Effective length of cushion Wetted area of side hulls at rest off cushion SSHO Wetted area of side hulls under way on cushion SSH Wetted area of side hulls under way off cushion Horizontal spacing between inner and outer side skirt hinges or attachment points to structure Distance of leading skirt contact point out-board or outer hinge of attachment points to structure Vertical spacing between inner and outer side skirt hinges or attachment points to structure Vertical spacing between inner and outer side skirt hinges or attachment points to structure Vertical spacing between inner and outer side skirt hinges or attachment points to structure Vertical spacing between inner and outer side skirt hinges or attachment points to structure Vertical spacing between inner and outer side skirt hinges or attachment points to structure Vertical spacing between inner and outer side skirt hinges or attachment points to structure Vertical spacing between inner and outer side skirt hinges or attachment points to structure Vertical spacing between inner and outer side skirt hinges or attachment points to structure Vertical spacing between inner and outer side skirt hinges or attachment points to structure Vertical spacing between inner and outer side skirt hinges or attachment points to structure Vertical spacing between inner and outer side skirt hinges or attachment point to structure Vertical spacing between inner and outer side skirt hinges or attachment point to structure Vertical spacing between inner and outer side skirt hinges or attachment point to structure Vertical spacing between inner and outer side skirt hinges or attachment point to structure Vertical spacing between inner and outer side skirt hinges or attachment point to structure	BCU Cushion breadth BWLT Total waterline breadth of SES Height of centre of gravity above mean water plane beneath craft HBS Bow seal height HSK Skirt depth HSS Stern seal height LB Deformed bag contact length LAC Cushion length LAC Effective length of cushion SSHO Wetted area of side hulls under way on cushion Wetted area of side hulls under way on cushion SSHC Wetted area of side hulls under way on cushion Wetted area of side hulls under way of cushion Horizontal spacing between inner and outer side skirt hinges or attachment points to structure Distance from side wall keel to lower edge of bow seal Ac/BC Total wetted area of side walls under way on cushion Total wetted area of side walls under way of cushion Total wetted area of side walls under way off cushion Ac way off cushion Total wetted area of side walls under way off cushion Total wetted area of side walls under way off cushion Ac way off cushion Total wetted area of side walls under way off c

ITTC

Symbol

3.4 ACV and SES3.4.1 Geometry and Hydrostatics

Computer	Nama	Definition or	SI-
Symbol	Name	Explanation	Unit

3.4.2 Resistance and Propulsion

		on Hull Resistance	2/2:	-
C <u>a</u>	CLOAD	Cushion loading coefficient	$\Delta / (g \rho_{\rm A} A_{\rm C}^{3/2})$	1
$C_{ m PR}$	CPR	Aerodynamic profile drag coefficient	$R_0 / (\rho_{\rm A} V_{\rm R}^2 A_{\rm C}/2)$	1
Cwc	CWC	Cushion wave making coefficient		1
$o_{ m B}$	PBM	Mean bag pressure		Pa
$ ho_{ m BS}$	PBS	Bow seal pressure	Pressure in the bow seal bag	Pa
CE	PCE	Mean effective skirt pressure		Pa
CU	PCU	Cushion pressure	Mean pressure in the cushion	Pa
p_{FT}	PFT	Fan total pressure		Pa
$\mathcal{O}_{\mathrm{LR}}$	PLR	Cushion pressure to length ratio	$P_{ m CU}/L_{ m C}$	Pa/m
9sk	PSK	Skirt pressure in general		Pa
oss .	PSS	Stern seal pressure	Pressure in the stern seal bag	Pa
P _{FCU}	PFCU	Power of lift fan		W
P _{FSK}	PFSK	Power of skirt fan		W
Q_{BS}	QBS	Bow seal air flow rate	Air flow rate to the bow seal	m^3/s
Q_{CU}	QCU	Cushion air flow rate	Air flow rate to cushion	m^3/s
Q_{SS}	QSS	Stern seal air flow rate	Air flow rate to the stern seal	m^3/s
Qss Qt Qts	QT	Total air volume flow		m^3/s
Q_{TS}	QTS	Total air volume flow of skirt		m^3/s
R_{AT}	RAT	Total aerodynamic resistance	$R_M + R_0$	N
$R_{ m H}$	RH	Hydrodynamic resistance	$R_{ m W}+R_{ m WET}$	N
R_M	RM	Intake momentum resistance in general	$ ho_{ m A}Q_{ m T}V_{ m A}$	N
R_{MCU}	RMCU	Intake momentum resistance of cushion	$ ho_{ m A}Q_{ m CU}V_{ m A}$	N
R_{ASK}	RASK	Intake momentum resistance of skirt	$ ho_{ m A}Q_{ m TS}V_{ m A}$	N
R _{WET}	RWET	Resistance due to wetting		N
$T_{\rm C}$	TC0	Cushion thrust		N

	9 9
3.5.1	Resistance and Propulsion

ITTC	Computer	Nome	Definition or	SI-
Symbol	Symbol	Name	Explanation	Unit

3.5 Ice Going Vessels

3.5.1

Resistance and Propulsion (See Figure 3.4, p 225 and Figure 3.8, p 231 of Vol. 1 of the *Proceedings of the 21st ITTC*)

$C_{\rm I}$	CI	and Figure 3.8, p 231 of Vol. 1 of the <i>F</i> Coefficient of net ice resistance	$R_{\rm I} / (\rho_{\rm I} g h^2 B)$	1
C_{IW}	CIW	Coefficient of water resistance in the presence of ice	$R_{\rm IW}$ / (S $q_{\rm IW}$)	1
$F_{ m IN}$	FNIC	Normal ice force on a body	Projection of hull - ice interaction force on the external normal	N
$F_{ m IT}$	FTIC	Tangential ice force on a body	Projection of the hull - ice interaction force on the direction of motion	N
$Fr_{ m I}$	FNIC	Froude number based on ice thickness	$V/(g h_1)^{1/2}$	1
$F_{X\mathrm{I}} \ F_{Y\mathrm{I}} \ F_{Z\mathrm{I}}$	FXIC FYIC FZIC	Components of the local ice force		N N N
f id	CFRD	Coefficient of friction between surface of body and ice (dynamic)	Ratio of tangential force to normal force between two bodies (dynamic condition)	1
<i>f</i> is	CFRS	Coefficient of friction between surface of body and ice (static)	The same as above (static condition)	1
h_{I}	HTIC	Thickness of ice		m
h_{SN}	HTSN	Thickness of snow cover		m
K_{QIA}	KQICMS	Average coefficient of torque in ice	$Q_{IA} / (\rho_{\rm W} n_{IA}^2 D^5)$	1
K_{TIA}	KTICMS	Average coefficient of thrust in ice	$T_{IA}/(\rho_{\rm W} n_{IA}^2 D^4)$	1
n_{IA}	FRICMS	Average rate of propeller revolution in ice		Hz
$P_{ m DI}$	PDI	Delivered power at propeller in ice	$2 \pi Q_{\text{IA}} n_{\text{IA}}$	W
Q_{IA}	QIMS	Average torque in ice		Nm
$R_{\rm I}$	RI	Net ice resistance	$R_{ m IT}$ - $R_{ m IW}$	N
$R_{\rm IT}$	RIT	Total resistance in ice	Ship towing resistance in ice	N
R_{IW}	RIW	Hydrodynamic resistance in presence of ice	Total water resistance of ship in ice	N
T_{IA}	TIMS	Average total thrust in ice		N
$\eta_{ m ICE}$	ERIC	Relative propulsive efficiency in ice	$\eta_{ m ID}/\eta_{ m D}$	1
$\eta_{ ext{ID}}$	EFDIC	Propulsive efficiency in ice	$R_{\rm IT} V / (2 \pi n_{\rm IA} Q_{\rm IA})$	1

3 Special Craft 3.6 Sailing Vessels 3.6.1 Geometry and Hydrostatics

ITTC	Computer	Nome	Definition or	SI-
Symbol	Symbol	Name	Explanation	Unit

3.6 Sailing Vessels

3.6.1 Geometry and Hydrostatics See also Section 2.2.1 on Hull Geometry

260	e also Section 2.2.1	2		
$A_{ m J}$	ASJ	Area of jib or genoa		m^2
$A_{ m LK}$	ALK	Lateral area of keel		m^2
$A_{ m LT}$	ALT	Total lateral area of yacht		m^2
$A_{ m m}$	ASM	Area of mainsail		m^2
$A_{ m N}$	ASN	Normalized sail area		m^2
$A_{\rm SP}$	ASSP	Area of spinnaker		m^2
$A_{\rm S}$, S_A	AS	Sail area in general	(P E + I J) / 2	m^2
B_{OA}	BOA	Breadth, overall		m
C_{pi}	CPI	Center of pressure for A _i Main-		
E	EM	sail base		m
I	I	Fore triangle height		m
J	J	Fore triangle base		m
P	P	Mainsail height		m
$L_{ m EFF}$	LEFF	Effective length for Reynolds Number		m
S_{C}	SC	Wetted surface area of canoe body		m ²
$S_{ m K}$	SK	Wetted surface area of keel		m^2
$S_{ m R}$	SR	Wetted surface area of rudder		m ²
$T_{ m C}$	TCAN	Draught of canoe body		m
$T_{ m EFF}$	TEFF	Effective draught	$F_{\rm H} / (\rho V_{\rm B}^2 R)^5$	m
Z_{CE}	ZCE	Height of centre of effort of sails above waterline in vertical centre plane		m
$V_{ m C}$	DVCAN	Displaced volume of canoe body		m^3
$V_{\rm K}$	DVK	Displaced volume of keel		m^3
$V_{\rm R}$	DVR	Displaced volume of rudder		m^3
Δ_{C}	DFCAN	Displacement force (weight) of canoe body		N
Δ_{K}	DFK	Displacement force (weight) of keel		N
Δ_{R}	DFR	Displacement force (weight) of rudder		N

3 Special Craft3.6 Sailing Vessels3.6.2 Resistance and Propulsion

ITTC Symbol	Computer Symbol	Name	Definition or Explanation	SI- Unit
Symbol	Syllibol		Explanation	Ollit
3.6.2 Res	istance and Prop	pulsion		
	1	Frictional resistance coefficient	D //G)	4
$C_{ m FU}$	CFU	(upright)	$R_{\mathrm{FU}} / (S q)$	1
C	CRU	Residuary resistance coefficient	$D = /(C \alpha)$	1
C_{RU}	CKU	(upright)	$R_{\mathrm{RU}} / (S q)$	1
C_{TU}	CTU	Total resistance coefficient (upright)	$R_{\mathrm{TU}} / (S q)$	1
$C_{ m WU}$	CWU	Wave resistance coefficient (upright)		1
$C_{\mathrm{T} arphi}$	СТРНІ	Total resistance coefficient with heel and leeway	$R_{\mathrm{T}\varphi} / (S q)$	1
C_{I}		Induced resistance coefficient		1
C_x , C_y , C_z		Force coefficients		1
$F_{ m H}$		Heeling force of sails		N
F_{R}		Driving force of sails		N
$F_{ m V}$		Vertical force of sails		N
Н		Side force		N
$L_{ m HY}$		Hydrodynamic lift force		N
$R_{ m AW}$		Mean added resistance in waves		N
$R_{ m FU}$		Friction resistance (upright)		N
$R_{ m RU}$		Residuary resistance (upright)		N
$R_{ m I}$		Resistance increase due to side		N
		(induced resistance)		11
R_{TU}	RTU	Total resistance (upright)		N
$R_{T\varphi}$	RTUH	Total resistance when heeled	$R_{ m TU}+R_{arphi}$	N
R_{arphi} , $R_{ m H}$	RTUHA	Resistance increase due to heel (with zero side force)		N
X,Y,Z		Components of resultant force along designated axis		N
V	V	Vessel velocity		m/s
$V_{ m WR}$	VWR	Apparent wind velocity		m/s
$V_{ m WT}$	VWT	True wind velocity		m/s
$V_{ m mc}$	VMC	Velocity made good on course		m/s
$V_{ m mg}$	VMG	Velocity made good to windward		m/s
		(contrary to wind direction)		
$eta_{ m L}$	BETAL	leeway angle		rad
$oldsymbol{eta}_{ m aw}$	BETWA	apparent wind angle (relative to boat course)		rad
$eta_{ m tw}$	BETWT	true wind angle (relative to boat course)		rad

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4. BACKGROUND AND REFERENCES

4.1 Symbols and Terminology Group

The tasks of the former Symbols and Terminology Group (SaT) have been handed over to the Quality Systems Group in 2002.

4.2 Description of the List of Symbols

4.2.1 Classification

The prime concern of the QS Group was to revise and try to complement the list of ITTC Standard Symbols sticking to the system for the classification of concepts.

With this regard, the following design requirements and goals have been maintained:

- 1. a coherent document, meeting the present and possibly the future requirements of the ITTC community in general and particular user groups
- 2. an open ended matrix structure that can be easily expanded as requirements arise, without the need of restructuring and repetition or too many explicit cross-references
- 3. minimized departures from the well established and widely accepted previous list of symbols

On the other hand, to facilitate the practical use of the list, a second version in which the symbols are arranged in alphabetic order was prepared. Symbols which have been listed several times in the matrix structured document have been maintained and for each symbol the field in which it is used is given in italic letters prior to the meaning of the symbol.

4.2.2 Structure of the Lists

The concepts related to a given subject area or model are designated by the ITTC Symbol and called by their Name. Their meaning can in principle only be concluded from the context of the model. The logically consistent, so called 'implicit' definition is derived from a definitely defined statement of the model, ideally a generally accepted system or an equivalent, e.g. a drawing.

The problem is that traditionally in lists of symbols, as in dictionaries, these explicit models are missing for various reasons. One reason is that many subject areas under discussion are far from being developed and understood to the extent necessary. A consequence of this situation is that the symbols proposed are not always as coherent as would be necessary for advanced and systematic work, for which explicit models and adequate notations are essential.

The problem under discussion is of course the same in national and international standards. However there is an accepted international standard which deals with the general principles concerning physical quantities, equations, quantity and unit symbols, and coherent unit systems for general use within the various fields of science and technology (ISO 31.

4.2.3 Organization of the matrix structured list

As has been emphasized the development of symbols is a continuing process and as the subject develops, further amendments and additions, as approved by the Conference, will be included in future editions of the list.

In order to avoid any extra problems the symbols are arranged in alphabetical order in each subject area as in previous lists. Continuous page numbering was discarded in earlier versions. The idea was to establish a loose leaf organization as the most appropriate, in view of new draughts to be incorporated.

In view of the tremendous effort which explicit mathematical models, explanations, and sketches take for their preparation, the present QS Group can only follow the former SaT Group and state that the Technical Committees and other interested parties are urged to provide further material for review by the QS Group and future inclusion into the list.

It has been noted that some users dislike the disruption of the list of symbols by lengthy explanations. The present QS Group feels that the subject and the sensible use of the symbols require such explanations, also as the fundamentals of the theory of science and terminology often are not taught to students of naval architecture and marine engineering. However the arrangement has been changed so that these explanations can be visited by using hyperlinks and the list is not disrupted any more.

5. PRINCIPLES OF NOTATION

In Figure 5 the principles of notation in according to ISO 31 are shown.

Symbols representing physical quantities normally are one Latin or Greek letter with Subscripts for further identification. They are written in *italic* style letters.

Numbers are normally written in **roman** style letters. For more details, look at the list below or in the Excerpts of ISO 31 below or in standard itself.

Superscripts signify operators e.g.

- exponentiation
- the various aspects of complex quantities
- the various aspects of spectra and
- the various aspects of random quantities and stochastic processes e.g. probability operators.

Subscripts signify identifiers

- matrix components,
- identifiers tested, e.g. ship S or model M, appendages (App)or the various bodies in a multi-body problem,
- identifiers of coordinate systems and of the reference points, quantities(L_{PP})

Symbols for physical units	italic, one letter, except dimensionless quanti-	A (e.g. Area in m ²)
	ties	
Symbols for characteristic numbers	2 letters italic	Re, Fr
Numbers	roman, generally	10^{3}
Symbols representing numbers	italic	χ_{ij}
Units	roman, lower case unless derived from name	m, Pa
Prefix of units	roman	μm
Symbols for chemical elements	roman	H_2O
Symbols for universal constants	italic	$g = 9,80665 \text{ m/s}^2$

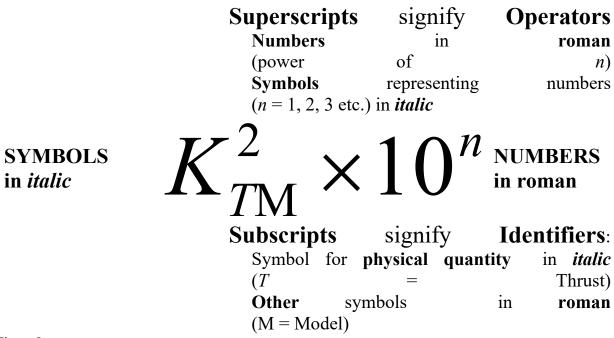


Figure 5

5.1 Excerpts of ISO 31

1 Scope

This part of ISO 31 gives general information about principles concerning physical quantities, equations, quantity and unit symbols, and coherent unit systems, especially the International System of Units, SI.

The principles laid down in this part of ISO 31 are intended for general use within the various fields of science and technology and as a general introduction to the other parts of ISO 31.

2. Quantities and units

2.1 Physical quantity, unit and numerical value

In ISO 31 only physical quantities used for the quantitative description of physical phenomena are treated. Conventional scales, such as the Beaufort scale, Richter scale and colour intensity scales, and quantities expressed as the results of conventional tests, e.g. corrosion resistance, are not treated here, neither are currencies nor information contents.

Physical quantities may be grouped together into categories of quantities which are mutually comparable. Lengths, diameters, distances, heights, wavelengths and so on would constitute such a category. Mutually comparable quantities are called "quantities of the same kind".

If a particular example of a quantity from such a category is chosen as a reference quantity, called the *unit*, then any other quantity from this category can be expressed in terms of this unit as a product of this unit and a number. This number is called the *numerical value* of the quantity expressed in this unit.

In formal treatments of quantities and units, this relation may be expressed in the form

$$A=\{A\}-[A]$$

where A is the symbol for the physical quantity, [A] the symbol for the unit and {A} symbolizes the numerical value of the quantity A expressed in the unit [A]. For vectors and tensors the components are quantities which may be expressed as described above.

If a quantity is expressed in another unit which is k times the first unit, then the new numerical value becomes 1/k times the first numerical value; the physical quantity, which is the product of the numerical value and the unit, is thus independent of the unit.

REMARK ON NOTATION FOR NUMERICAL VALUES

It is essential to distinguish between the quantity itself and the numerical value of the quantity expressed in a particular unit. The numerical value of a quantity expressed in a particular unit could be indicated by placing braces (curly brackets) around the quantity symbol and using the unit as a subscript. It is, however, preferable to indicate the numerical value explicitly as the ratio of the quantity to the unit.

2.2 Quantities and equations

2.2.1 Mathematical operations with quantities

Two or more physical quantities cannot be added or subtracted unless they belong to the same category of mutually comparable quantities.

Physical quantities are multiplied or divided by one another according to the rules of algebra; the product or the quotient of two quantities, *A* and *B*, satisfies the relations

$$AB = \{A\} \{B\} - [A] [B]$$

Thus, the product $\{A\}$ $\{B\}$ is the numerical value $\{AB\}$ of the quantity AB, and the product [A] [B] is the unit [AB] of the quantity AB. Similarly, the quotient $\{A!/\{B\}\}$ is the numerical value $\{A/B\}$ of the quantity A/B, and the quotient [A]/[B] is the unit [A/B] of the quantity A/B.

2.2.2 Equations between quantities and equations between numerical values

Two types of equation are used in science and technology: *equations between quantities*, in which a letter symbol denotes the physical quantity (i.e. numerical value × unit), and *equations between numerical values*. Equations between numerical values depend on the choice of units, whereas equations between quantities have the advantage of being independent of this choice. Therefore the use of equations between quantities should normally be preferred.

2.2.3 Empirical constants

An empirical relation is often expressed in the form of an equation between the numerical values of certain physical quantities. Such a relation depends on the units in which the various physical quantities are expressed.

An empirical relation between numerical values can be transformed into an equation between physical quantities, containing one or more empirical constants. Such an equation between physical quantities has the advantage that the form of the equation is independent of the choice of the units. The numerical values of the empirical constants occurring in such an equation depend, however, on the units in which they are expressed, as is the case with other physical quantities.

2.2.4 Numerical factors in quantity equations

Equations between quantities sometimes contain *numerical factors*. These numerical factors depend on the definitions chosen for the quantities occurring in the equations

EXAMPLE

$$E_k = \frac{1}{2} m v^2$$

2.2.5 Systems of quantities and equations between quantities; base quantities and derived quantities

Physical quantities are related to one another through equations that express laws of nature or define new quantities.

For the purpose of defining unit systems and introducing the concept of dimensions, it is convenient to consider some quantities as mutually independent, i.e. to regard these as *base quantities*, in terms of which the other quantities can be defined or expressed by means of equations; the latter quantities are called *derived quantities*.

It is a matter of choice how many and which quantities are considered to be base quantities.

The whole set of physical quantities included in ISO 31 is considered as being founded on seven base quantities: length L, mass M, time T, electric current I, thermodynamic temperature Θ , amount of substance N and luminous intensity J.

In the field of mechanics a system of quantities and equations founded on three base quantities is generally used. In ISO 31-3, the base quantities used are length, mass and time.

In the field of electricity and magnetism a system of quantities and equations founded on four base quantities is generally used. In ISO 31-5, the base quantities used are length, mass, time and electric current.

In the same field, however, systems founded on only three base quantities, length, mass and time, in particular the "Gaussian" or symmetric system, have been widely used. (See ISO 31-5:1992, annex A.)

2.2.6 Dimension of a quantity

Any quantity Q can be expressed in terms of other quantities by means of an equation. The expression may consist of a sum of terms. Each of these terms can be expressed as a product of powers of base quantities A, B, C, ... from a chosen set, sometimes multiplied by a numerical factor ξ , i.e. $\xi A^{\alpha}B^{\beta}C^{\gamma}$..., where the set of exponents $(\alpha, \beta, \gamma$...) is the same for each term.

The *dimension* of the quantity Q is then expressed by the dimensional product

$$\dim Q = A^{\alpha}B^{\beta}C^{\gamma} ...$$

where A, B, C, ... denote the dimensions of the base quantities A, B, C, ..., and where α , β , γ are called the **dimensional exponents**.

A quantity all of whose dimensional exponents are equal to zero is often called a *dimensionless* quantity. Its dimensional product or dimension is $A^0 B^0 C^0 ... = 1$. Such a quantity of *dimension one* is expressed as a number.

In the system founded on the seven base quantities length, mass, time, electric current, thermodynamic temperature, amount of substance and luminous intensity, the base dimensions may be denoted by L, M, T, I, O, N and J respectively and the dimension of a quantity Q becomes in general

 $\dim Q = L^{\alpha} M^{\beta} T^{\gamma} I^{\delta} \Theta^{\varepsilon} N^{\zeta} J^{\eta}.$

EXAMPLES

Quantity	Dimension
velocity	LT ⁻¹
angular velocity	T ⁻¹
force	LMT ⁻²
energy	L^2MT^{-2}
relative density	1

2.3 Units

2.3.1 Coherent unit systems

Units might be chosen arbitrarily, but making an independent choice of a unit for each quantity would lead to the appearance of additional numerical factors in the equations between the numerical values.

It is possible, however, and in practice more convenient, to choose a system of units in such a way that the equations between numerical values have exactly the same form (including the numerical factors) as the corresponding equations between the quantities. A unit system defined in this way is called *coherent* with respect to the system of quantities and equations in question. The SI is such a system. The corresponding system of quantities is given in ISO 31-1 to ISO 31-10 and in ISO 31-12 and ISO 31-13.

For a particular system of quantities and equations, a coherent system of units is obtained by first defining units for the base quantities, the *base units*. Then for each derived quantity, the definition of the corresponding *derived unit* in terms of the base units is given by an algebraic expression obtained from the dimensional product (see 2.2.6) by replacing the symbols for the base dimensions by those of the base units. In particular, a quantity of dimension one acquires the unit 1. In such a coherent unit system no numerical factor other than the number 1 ever occurs in the expressions for the derived units in terms of the base units.

2.3.2 SI units and their decimal multiples and sub-multiples

The name *International System of Units* (Système International d'Unités), with the international abbreviation SI was adopted by the 11th

General Conference on Weights and Measures (Conférence Générale des Poids et Mesures, CGPM) in 1960.

This system includes

- base units
- derived units including supplementary units which together form the coherent system of *SI units*.

2.3.2.1 Base units

The seven base units are listed in Table 1.

Table 1 - SI base units

	SI base unit		
Base quantity	Name	Symbol	
length	metre	m	
mass	kilogram	kg	
time	second	S	
electric current	ampere	A	
thermodynamic tempera- ture	kelvin	K	
amount of substance	mole	mol	
luminous intensity	candela	cd	

2.3.2.2 Derived units including supplementary units

The expressions for the coherent derived units in terms of the base units can be obtained from the dimensional products by using the following formal substitutions:

$L \rightarrow m$	$I \rightarrow A$
$M \rightarrow kg$	$\Theta \to K$
$T \rightarrow s$	$N \rightarrow mol$
	$I \rightarrow cd$

In 1960, the CGPM classified the SI units radian, rad, and steradian, sr, for plane angle and solid angle respectively as "supplementary units".

In 1980, the *International Committee for Weights and Measures* (Comité International des Poids et Mesures, CIPM) decided to interpret the class of supplementary units in the SI as a class of dimensionless derived units for which the CGPM allows the freedom of using or not using them in expressions for SI derived units.

Although, as a consequence of this interpretation, the coherent unit for plane angle and for solid angle is the number 1, it is convenient to use the special names radian, rad, and steradian, sr, instead of the number 1 in many practical

Table 2 - SI derived units with special names, including SI supplementary units

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	SI derived unit		
Derived quantity	Special name	Symbol	Expressed in terms of SI base units and SI derived units
plane angle	radian	rad	1 rad = 1 m/m = 1
solid angle	steradian	sr	$1 \text{ sr} = 1 \text{ m}^2 / \text{m}^2 = 1$
frequency	hertz	Hz	$1 \text{ Hz} = 1 \text{ s}^{-1}$
force	newton	N	$1 \text{ N} = 1 \text{ kg} \cdot \text{m/s}^2$
pressure,	pascal	Pa	$1 \text{ Pa} = 1 \text{ N/m}^2$
stress			
energy,	joule	J	1 J = 1 N - m
work,			
quantity of heat		***	1 337 1 1/
power, radiant flux	watt	W	1 W = 1 J/s
electric charge,	coulomb	С	1 C = 1 A - s
quantity of electricity	Coulomb		TC TA-S
electric potential,	volt	V	1 V = 1 W/A
potential difference,			
tension,			
electromotive force			
capacitance	farad	F	1 F = 1 C/V
electric resistance	ohm	S2	$1\Omega = 1 \text{ V/A}$
electric conductance	siemens	S	$1 S = 1 \Omega^{-1}$
magnetic flux	weber	Wb	1 Wb = 1 V . s
magnetic flux density	tesla	T	$1 T = 1 Wb/m^2$
inductance	henry	Н	1 H = 1 Wb/A
Celsius temperature	degree	°C	1 °C = 1 K
_	Celsius')		
luminous flux	lumen	Im	1 lm = 1 cd. sr
illuminance	lux	Ix	1 lx = 1 lm/m2

1) Degree Celsius is a special name for the unit kelvin for use in stating values of Celsius temperature. (See also ISO 31-4:1992, items 4-1.a and 4-2.a.)

EXAMPLES

Quantity

Symbol for SI unit expressed in terms of the seven base units (and the supplementary units in some cases)

velocity	m/s
angular velocity	rad/s or s ⁻ '
force	$kg \cdot m/s^2$
energy	$kg \cdot m^2/s^2$
relative density	1

For some of the SI derived units, special names and symbols exist; those approved by the CGPM are listed in tables 2 (and 3).

It is often of advantage to use special names and symbols in compound expressions for units.

2.3.2.3 SI prefixes

In order to avoid large or small numerical values, decimal multiples and sub-multiples of the SI units are added to the coherent system within the framework of the SI. They are formed by means of the prefixes listed in Table 4

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Table 4 - Sl prefixes

Factor	Prefix	
	Name	Symbol
10^{24}	yotta	Y
10^{2I}	zetta	Z
1018	exa	Е
10^{15}	peta	P
10^{12}	tera	T
10^{9}	giga	G
106	mega	M
10^{3}	kilo	k
10^{2}	hecto	h
10	deca	da
10-1	deci	d
10-2	centi	c
10-3	milli	m
10-6	micro	μ
10-9	nano	n
10-12	pico	p
10-15	femto	f
10-18	atto	a
10-21	zepto	Z
10-24	yocto	у

For information about the use of the prefixes, see 3.2.4.

The SI units and their decimal multiples and submultiples formed by use of the prefixes are specially recommended.

2.3.3 The unit one

The coherent SI unit for any quantity of dimension one is the unit one, symbol 1. It is generally not written out explicitly when such a quantity is expressed numerically.

EXAMPLE

Refractive index $n = 1,53 \times 1 = 1,53$

In the case of certain such quantities, however, the unit 1 has special names that could be used or not, depending on the context.

EXAMPLES

Plane angle
$$\alpha=0.5 \, {\rm rad}$$
 = 0.5 rad = 0.5 solid angle $\Omega=2.3 \, {\rm sr}$

Decimal multiples and sub-multiples of the unit one are expressed by powers of 10. They shall not be expressed by combining the symbol 1 with a prefix.

In some cases the symbol % (per cent) is used for the number 0,01.

NOTES

3 In some countries the symbol %0 ("per mill", or per thousand) is used for the number 0,001. This symbol should be avoided.

Since per cent and per mill are numbers it is in principle meaningless to speak about percentage by mass or percentage by volume. Additional information, such as % (m/m) or % (V/V), should not therefore be attached to the unit symbol. The preferred way of expressing a mass fraction is: "the mass fraction is 0,67" or "the mass fraction is 67 %", and the preferred way of expressing a volume fraction is: "the volume fraction is 0,75" or "the volume fraction is 75 %". Mass and volume fractions can also be expressed in the form $5 \mu g/g$ or 4,2 ml/m3.

Abbreviations such as ppm, pphm and ppb shall not be used.

2.3.4 Other unit systems and miscellaneous units

The CGS system of mechanical units is a coherent system the base units of which are centimetre, gram and second for the three base quantities length, mass and time.

In practice this system was enlarged by adding the kelvin, the candela and the mole as base units for the base quantities thermodynamic temperature, luminous intensity and amount of substance.

Units used in electricity and magnetism have been defined in the CGS system in several ways depending on the system of quantities and equations chosen. The "Gaussian" or symmetric CGS system, coherent with the "Gaussian" or symmetric system of quantities and equations founded on three base quantities, has been widely used. For further information on this system, see ISO 31-5:1992, Annex A.

The special names and symbols for derived CGS units such as dyne, erg, poise, stokes, gauss, oersted and maxwell shall not be used together with the Sl.

Table 5 - Units used with the SI

Quantity	Unit			
	Name	Symbol	Definition	
time	minute hour day	min h d	1 min= 60s 1 h = 60 min 1 d = 24 h	
plane angle	degree minute second	° ' ' ' ' ' ' ' ' ' ' ' ' ' ' ' ' ' ' '	1°= (π/180)rad = (n/180) rad 1'= (1/60)° 1"= (1/60)'	
volume	litre	I, L 1)	$11 = 1 \text{ dm}^3$ = 1 dm	
mass	tonne ²⁾	t	$1 t = 10^3 kg$	
1) The two symbols for litre are on an equal footing. The				

¹⁾ The two symbols for litre are on an equal footing. The CIPM will, however, make a survey on the development

of the use of the two symbols in order to see if one of the two may be suppressed.

²⁾ Also called the metric ton in the English language.

Table 6 - Units used with the SI, whose values in SI units are obtained experimentally

a	Unit			
Quantity	Name	Symbol	Definition	
energy	electronvolt	eV		
			The electronvolt is the kinetic energy acquired by an electron in passing through a potential difference of 1 volt in vacuum: 1 eV \approx 1,602 177 \times 10 ⁻¹⁹ J.	
mass	unified atomic mass unit	u	The unified atomic mass unit is equal to $(1/12)$ of the mass of an atom of the nuclide ¹² C: 1u \approx 1,660 540 \times 10 ⁻²⁷ kg.	

In other parts of ISO 31, the special names for the derived CGS units are given in informative annexes which are not integral parts of the standards.

There are certain units outside the SI which are recognized by the CIPM as having to be retained for use together with the SI, e.g. minute, hour and electronvolt. These units are given in Tables 5 and 6.

Other coherent systems of units have been defined, e.g. a system based on the units foot, pound and second and a system based on the units metre, kilogram-force and second.

Apart from these, other units have been defined which do not belong to any coherent system, e.g. the atmosphere, **the nautical mile** and the curie.

3 Recommendations for printing symbols and numbers

3.1 Symbols for quantities

3.1.1 Symbols

The symbols for physical quantities are generally single letters of the Latin or Greek alphabet, sometimes with subscripts or other modifying signs. These **symbols** are printed in *italic* (sloping) type (irrespective of the type used in the rest of the text).

The symbol is not followed by a full stop except for normal punctuation, e.g. at the end of a sentence.

NOTES

5 Symbols for quantities are given in ISO 31-1 to ISO 31-10 and in ISO 31-12 and ISO 31-13.

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- 6 Notations for vectorial and other non-scalar quantities are given in ISO 31-11, on mathematical signs and symbols
- 7 Exceptionally, symbols made up of two letters are sometimes used for combinations of dimension one of quantities (e.g. Reynolds number, *Re*). If such a two-letter symbol appears as a factor in a product, it is recommended that it be separated from the other symbols.

3.1.2 Rules for the printing of subscripts

When, in a given context, different quantities have the same letter symbol or when, for one quantity, different applications or different values are of interest, a distinction can be made by use of subscripts.

The following principles for the printing of subscripts are recommended:

A subscript that represents a symbol for a physical quantity is printed in italic (sloping) type.

Other subscripts are printed in roman (upright) type.

EXAMPLES

Uprig	Upright subscripts Sloping subscripts		
$oldsymbol{C}_{ ext{g}}$	(g gas)	C_p	(p: pressure)
g_n	(n: normal)	$\sum_n a_n \delta_n$	(n: running num-
			ber)
$\mu_{\rm r}$	(r: relative)	$\sum_{x} a_{x} b_{x}$	(x: running num-
			ber)
$oldsymbol{E}_{\mathbf{k}}$	(k: kinetic)	g_{ik}	(i, k: running num-
			bers)
χe	(e: electric)	p_x	(x:x-coordinate)
$T_{1/2}$	(1/2: half)	l_{λ}	$(\lambda \text{ wavelength})$

NOTES

8 Numbers as subscripts should be printed in roman (upright type. However, letter symbols representing numbers are generally printed in italic (sloping) type.

3.1.3 Combination of symbols for quantities; elementary Operations with quantities

When symbols for quantities are combined in a product, this process of combination may be indicated in one of the following ways:

$$ab$$
, ab , $a \cdot \bullet b$, $a \times b$

NOTES

10 In some fields, e.g. in vector analysis, distinction is made between $\mathbf{a} \cdot \mathbf{b}$ and $\mathbf{a} \times \mathbf{b}$.

11 For multiplication of numbers, see 3.3.3.

12 In systems with limited character sets a dot on the line may be used instead of a half-high dot.

Division of one quantity by another may be indicated in one of the following ways:

$$\frac{a}{b}$$
, a/b or by writing the product of **a** and **b**⁻¹,

e.g. *a*·· *b*-1

3.2 Names and symbols for units

3.2.1 International symbols for units

When international symbols for units exist, they, and no other, shall be used. They shall be printed in roman (**upright**) type (irrespective of the type used in the rest of the text), shall remain unaltered in the plural shall be written without a final full stop (period) except for normal punctuation, e.g. at the end of a sentence.

Any attachment to a unit symbol as a means of giving information about the special nature of the quantity or context of measurement under consideration is incorrect.

EXAMPLE

$$U_{\text{max}} = 500 \text{ V} \text{ (not } U = 500 \text{ V}_{\text{max}} \text{)}$$

The unit symbols shall in general be printed in lower case letters except that the first letter is printed in upper case when the name of the unit is derived from a proper name.

EXAMPLES

m metre s second A ampere Wb weber

3.2.2 Combination of symbols for units

When a compound unit is formed by multiplication of two or more units, this should be indicated in one of the following ways:

N⋅m, N m

NOTES

13 In systems with limited character sets a dot on the line may be used instead of a half high dot.

14 The latter form may also be written without a space, provided that special care is taken when the symbol for one of the units is the same as the symbol for a prefix.

EXAMPLE

mN means millinewton, not metre newton.

When a compound unit is formed by dividing one unit by another, this should be indicated in one of the following ways:

$$\frac{m}{s}$$
 m/s m·s⁻¹

A solidus (/) shall not be followed by a multiplication sign or a division sign an the same line unless parentheses are inserted to avoid any ambiguity. In complicated cases negative powers or parentheses shall be used.

3.2.3 Printing of symbols for units

No recommendation is made or implied about the font of upright type in which symbols for units are to be printed.

NOTE 15 In this series of publications the font used in such cases is generally that of the associated text, but this does not constitute a recommendation.

3.2.4 Printing and use of prefixes

Symbols for prefixes should be printed in roman (upright) type without a space between the symbol for the prefix and the symbol for the unit.

Compound prefixes shall not be used.

EXAMPLE

Write nm (nanometre) for 10⁻⁹ m, not mµm.

The symbol of a prefix is considered to be combined with the single unit symbol to which it is directly attached, forming with it a new symbol (for a decimal multiple or sub-multiple) which can be raised to a positive or negative power, and which can be combined with other unit symbols to form symbols for compound units (see 3.2.2).

EXAMPLES

$$\begin{array}{l} 1cm^3 = (10^{\text{-2}}m)^3 {=} 10^{\text{-6}}\,m^3 \\ 1\;\mu\text{s}^{\text{-1}} {=}\; (10^{\text{-6}}\;\text{s})^{\text{-1}} {=}\; 10^6\;\text{s}^{\text{-1}} \\ 1\;k\text{A/m} {=}\; (10^3\text{A})/m {=}\; 10^3\;\text{A/m} \end{array}$$

NOTE 16 For historical reasons the name of the base unit or mass, the kilogram, contains the name of the SI prefix ,"kilo". Names of the decimal multiples and sub-multiples of the unit of mass are formed by adding the prefixes to the word ,,gram", e.g. milligram (mg) instead of microkilogram (μ kg).

3.3 Numbers

3.3.1 Printing of numbers

Numbers should generally be printed in roman (upright) type.

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To facilitate the reading of numbers with many digits, these may be separated into suitable groups, preferably of three, counting from the decimal sign towards the left and the right; the groups should be separated by a small space, and never by a comma or a point, or by any other means.

3.3.2Decimal sign

The decimal sign is a comma on the line.

If the magnitude of the number is less than unity, the decimal sign should be preceded by a zero.

NOTE 17 In documents in the English language. a dot is often used instead of a comma. If a dot is used, it should be on the line. In accordance with an ISO Council decision, the decimal sign is a comma in ISO documents.

3.3.3 Multiplication of numbers

The sign for multiplication of numbers is a cross (\times) or a dot half-high (\cdot).

NOTES

18 If a dot half-high is used as the multiplication sign, a comma should be used as the decimal sign. If a dot is used as the decimal sign, a cross should be used as the multiplication sign.

19. In ISO documents, the dot is not used directly between numbers to indicate multiplication.

3.4 Expressions for quantities

The symbol of the unit shall be placed after the numerical value in the expression for a quantity, leaving a space between the numerical value and the unit symbol. It should be noted that, in accordance with this rule, the symbol °C for degree Celsius shall be preceded by a space when expressing a Celsius temperature.

The only exceptions to this rule are for the units degree, minute and second for plane angle, in which case there shall be no space between the numerical value and the unit symbol.

If the quantity to be expressed is a sum or a difference of quantities then either parentheses shall be used to combine the numerical values, placing the common unit symbol after the complete numerical value, or the expression shall be written as the sum or difference of expressions for the quantities.

EXAMPLES

l = 12 m - 7 m = (12 - 7) m = 5 m $t = 28.4 \text{ °C} \pm 0.2 \text{ °C} = (28.4 \pm 0.2) \text{ °C}$ (not $28.4 \pm 0.2 \text{ °C}$) $\lambda = 220 \times (1 \pm 0.02) \text{ W/(m·K)}$

3.5 Symbols for chemical elements and nuclides

Symbols for chemical elements shall be written in roman (upright) type (irrespective of the type used in the rest of the text). The symbol is not followed by a full stop except for normal punctuation, e.g. at the end of a sentence.

EXAMPLES

H He C Ca

A complete list of the symbols for the chemical elements is given in ISO 31-8:1992, annex A, and 150 31-9:1992, annex A.

The attached subscripts or superscripts specifying a nuclide or molecule shall have the following meanings and positions.

The nucleon number (mass number) of a nuclide is shown in the left superscript position, e.g. ¹⁴N

The number of atoms of a nuclide in a molecule is shown in the right subscript position, e.g. $^{14}\mathrm{N}_{2}$

The proton number (atomic number) may be indicated in the left subscript position, e.g. $_{64}\mathrm{Gd}$

If necessary, a state of ionization or an excited state may be indicated in the right superscript position.

EXAMPLES

State of ionization: Na⁺ $P O_{4}^{3-} \text{ or } (PO_{4})^{3-}$ Electronic excited state: He**, N0**
Nuclear excited state: $^{110}Ag^{*}$, $^{110}Ag^{m}$

3.6 Mathematical signs and symbols

Mathematical signs and symbols recommended for use in the physical sciences and technology are given in 1S031-11.

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Greek alphabet (upright and sloping types) **3.7**

alpha	Α	a	A	а
beta	В	β	В	β
gamma	Γ	δ	Γ	δ
delta	Δ	δ	Δ	δ
epsilon	E	3	E	ε
zeta	Z	ξ	Z	ε
eta	Н	η	H	η
theta	Θ	θ , \mathcal{G}	Θ	θ, Θ
iota	I	ι	I	ı
kappa	K	κ	K	κ
lambda	Λ	λ	Λ	λ
mu	M	μ	M	μ
nu	N	ν	N	v
xi	Ξ	ξ	Ξ	ζ
omicron	0	O	Ξ O	0
pi	П	π	П	π
rho	P	ρ	P Σ Τ	ρ ,
sigma	Σ	σ	Σ	σ
tau	P Σ Τ Υ	τ	T	τ
upsilon		υ	Y	v
phi	Φ	φ	Φ	φ
chi	X	χ	X	χ
psi	Ψ	Ψ	Ψ	Ψ
omega	Ω	ω	Ω	ω

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5.2 Computer Symbols

Wherever possible the symbols in the second column of the tables have been chosen so that their meaning is readily apparent. They have been constructed from the CCITT International Telegraph Alphabet, restricted character set. They are therefore suitable for use in a wide range of situations e. g.: Telex messages, letters, computer printouts etc.

To ensure that the symbols can be used in a wide range of programming languages they currently have been kept to less than six characters long. The symbols should be used as defined, and, in accordance with modern programming practice, should have their type explicitly declared before use. The following rules were applied in the derivation of the symbols:

- 1. Only upper case letter A Z and digits 0 9 have been used.
- 2. Formerly Greek letters have been spelled out, if necessary in abbreviated form or with changed spelling. This practice is considered obsolete.

- 3. The Froude 'circular' symbols are defined by the prefix CIRC.
- 4. All symbols start with a letter.
- 5. Qualifiers and operators, preferably two characters, are currently suffixed to the main symbol line, without spacing.
- 6. No one computer compatible symbol should be used for different concepts in a given context. This goal has not been completely achieved for the whole list. Ad hoc solutions have been attempted but discarded as unsatisfactory.
- 7. Since the computer compatible symbols have been proposed as the basis of attribute names for data exchanges, the above rules will probably be further developed in the near future.

A final remark on the Computer Symbols: in the computer, the letter O and figure 0 (zero) have fundamentally different meanings, but owing to their resemblance they can be easily confused. Thus it is necessary to distinguish rigorously between them. As a matter of fact there are contradictory conventions being widely used. <u>Version 2021</u> 103

5.3 Documentation

5.3.1 ITTC Documents

- 1. International Towing Tank Conference, Standard Symbols 1971, BSRA Technical Memorandum No.400, August 1971.
- International Towing Tank Conference, Standard Symbols 1976. BSRA T.M. No.500, 1976.
- 3. ITTC Dictionary of Ship Hydrodynamics. RINA Maritime Technology Monograph No.6, 1978.
- Translation of Overall Index of Titles of Dictionary of Ship Hydrodynamics., Vol. 1: CETENA, Genova, 1984,
 Vol. 2: University of Tokyo, 1984.
- 5. Bibliography and Proposed Symbols on Hydrodynamic Technology as Related Model Tests of High Speed Marine Vehicles. Prep. by 17th ITTC High-Speed Marine Vehicle Committee. SPPA Maritime Research and Consulting. Rep. No.101, 1984.

5.3.2 Translations

A number of translations of the List of ITTC Standard Symbols into languages other than English have been made including French, German, Italian, Japanese, Russian, Spanish and Chinese. For obvious reasons these translations are no longer up-to-date as the present accepted list in English and the Russian one.

- 1. French Translation of ITTC Standard Symbols 1971., Association Française de Normalisation (AFNOR).
- 2. International vereinbarte Buchstabensymbole und Bezeichnungen auf dem Gebiet der Schiffshydrodynamik. Collatz, G. Schiff und Hafen 27 (1975) No.10.
- 3. Italian Translation of ITTC Standard Symbols 1971. Luise E. Appendix II, Report of Presentation Committee. Proceedings 14th ITTC, Vol. 4, Ottawa 1975.

- 4. Japanese Translation of ITTC Standard Symbols. Transactions of the Society of Naval Architects of Japan, No.538, April 1974.
- Russian Translation of ITTC Standard Symbols 1971. Brodarski Institute Publication No.28, Zagreb 1974.
- Simbolos Internacionales en Arquitectura Naval. Asociacion de Investigacion de la Construccion Naval,
 - Publication 7/75, Juli 1975, Madrid.
- 7. Report of Information Committee, Proc. 17th ITTC, Göteborg 1984.
- 8. Chinese Translation of ITTC Standard Symbols. China Ship Scientific Research Centre, Wuxi.

5.3.3 Other References

Apart from the organizations represented on the ITTC these symbols have been recommended for use in technical writing on naval architecture by a number of organizations concerned with marine matters including The Royal Institution of Naval Architects, the American Society of Naval Architects and Marine Engineers and the American, British, Canadian, Australian, and Italian Navies. Where possible, the symbols for Section 3.4.1, Waves are consistent with the IAHR/PIANC List of Sea State Parameters, Supplement to Bulletin No 52, January 1986.

In 1985 the Draught International Standard ISO/DIS 7463 Shipbuilding - Symbols for Computer Applications - has been published. The symbols are based on the list approved by the ITTC in Ottawa 1975 and a related list produced by the ISSC in 1974, inconsistencies having been removed. The ISO/TC8/SC15 has been notified that major changes of the ITTC Symbols are under discussion. Subsequently processing of ISO/DIS 7463 has not been postponed, but the standard has been published as ISO 7463 in 1990.